No	Туре	Date	Room	Time	Start Time	Finish Time	Duration	Session ID	Session Title	Presentation ID	Submission no	Paper Title
1	Oral	November 26	Room A	14:30-16:30	14:30	14:45	0:15	IS	Industry Session	IS-1		TBD
2	Oral	November 26	Room A	14:30-16:30	14:45	15:15	0:30	IS	Industry Session	IS-2		TBD
3	Oral	November 26	Room A	14:30-16:30	15:15	15:45	0:30	IS	Industry Session	IS-3		TBD
4	Oral	November 26	Room A	14:30-16:30	15:45	16:30	0:45	IS	Industry Session	IS-4		TBD
5		November 27	Room A	9:30-10:00	9:30	10:00	0:30	ОР	Opening Ceremony	OP		
6	Oral	November 27	Room A	10:00-12:30	10:00	10:45	0:45	KS1	Keynote Session 1	KS1-1		Superconducting Maglev and Chuo Shinkansen
7	Oral	November 27	Room A	10:00-12:30	10:45	11:30	0:45	KS1	Keynote Session 1	KS1-2		Research on Power Electronics Technology for Future Power Grid
8	Oral	November 27	Room A	10:00-12:30	11:30	12:15	0:45	KS1	Keynote Session 1	KS1-3		Research on Permanent-Magnet Synchronous Machines with Hybrid Utilization of Permanent Magnets
9	Oral	November 27	Room A	14:30-16:00	14:30	15:15	0:45	KS2	Keynote Session 2	KS2-1		High Performance Integrated Motor Drives Using Wide Bandgap Devices Including Current Source Inverter
10	Oral	November 27	Room A	14:30-16:00	15:15	16:00	0:45	KS2	Keynote Session 2	KS2-2		Design and Manufacturing of MW-class High Performance Electrical Machines
11	Oral	November 27	Room B	16:20-18:20	16:20	16:40	0:20	OS1B	Induction Machines	OS1B-1	C000006	Compatibility Determination of Single-Phase Induction Motor and Load
12	Oral	November 27	Room B	16:20-18:20	16:40	17:00	0:20	OS1B	Induction Machines	OS1B-2	C000595	A Performance Analysis of a 12-Slot 10-Pole Concentrated Winding Induction Motor with Wave-Winding Rotor for Loss Reduction
13	Oral	November 27	Room B	16:20-18:20	17:00	17:20	0:20	OS1B	Induction Machines	OS1B-3	C000664	Equivalent Two-Dimensional Finite Element Analysis of Axial Flux Induction Motor with Double Stator and Single Rotor
14	Oral	November 27	Room B	16:20-18:20	17:20	17:40	0:20	OS1B	Induction Machines	OS1B-4	C000016	Controllability Enhancement of Doubly Fed Induction Generators by Use of Tapped Stator Windings
15	Oral	November 27	Room B	16:20-18:20	17:40	18:00	0:20	OS1B	Induction Machines	OS1B-5	C000143	Designing for Success: The Imperative of Critical Speed in Electrical Motors - Industry Perspective
16	Oral	November 27	Room B	16:20-18:20	18:00	18:20	0:20	OS1B	Induction Machines	OS1B-6	C000622	Influence of Rotor Closed Slots on Magnetic Field Harmonics and Electromagnetic Vibration in Induction Motors
17	Oral	November 27	Room C	16:20-18:20	16:20	16:40	0:20	OS1C	Permanent Magnet Machines 1	OS1C-1	C000390	Aluminum Windings and Their Manufacturing Technologies in Electrical Machines: A Review
18	Oral	November 27	Room C	16:20-18:20	16:40	17:00	0:20	OS1C	Permanent Magnet Machines 1	OS1C-2	C000341	Investigation of Reducing Magnet Amount in Traction Motors with Aluminum Windings
19	Oral	November 27	Room C	16:20-18:20	17:00	17:20	0:20	OS1C	Permanent Magnet Machines 1	OS1C-3	C000035	Layered Structure of Permanent Magnet for Eddy Current Loss Reduction in Electric Machine Design
20	Oral	November 27	Room C	16:20-18:20	17:20	17:40	0:20	OS1C	Permanent Magnet Machines 1	OS1C-4	C000688	Evaluation of an IPMSM Featuring a Rotor Core Directly Injection-Molded with Sm-Fe-N Bonded Magnets
21	Oral	November 27	Room C	16:20-18:20	17:40	18:00	0:20	OS1C	Permanent Magnet Machines 1	OS1C-5	C000292	A Study on Slot-Pole Combinations of Slit Stator Motors
22	Oral	November 27	Room C	16:20-18:20	18:00	18:20	0:20	OS1C	Permanent Magnet Machines 1	OS1C-6	C000820	Improving Reluctance Torque of Outer-Rotor- type PM Motor with Segmented Rotor Structure
23	Oral	November 27	Room D	16:20-18:20	16:20	16:40	0:20	OS1D	Reluctance Machines 1	OS1D-1	C000111	Standalone Testing Method of Synchronous Reluctance Motor for Determining Operating Characteristics
24	Oral	November 27	Room D	16:20-18:20	16:40	17:00	0:20	OS1D	Reluctance Machines 1	OS1D-2	C000766	Enhanced Performance of a Synchronous Reluctance Motor due to Less Rare-Earth Magnets Combined Ferrite and NdFeB
25	Oral	November 27	Room D	16:20-18:20	17:00	17:20	0:20	OS1D	Reluctance Machines 1	OS1D-3	C000903	A Novel Synchronous Reluctance Machine with Unequal-Turn Concentric Winding
26	Oral	November 27	Room D	16:20-18:20	17:20	17:40	0:20	OS1D	Reluctance Machines 1	OS1D-4	C000306	Research on High-speed PM-assisted Synchronous Reluctance Motor based on Dual- phase Materials
27	Oral	November 27	Room D	16:20-18:20	17:40	18:00	0:20	OS1D	Reluctance Machines 1	OS1D-5	C000175	Characteristics Analysis of a Novel Permanent Magnet Assisted 12/8 Segmental Rotor Type Switched Reluctance Motor
28	Oral	November 27	Room D	16:20-18:20	18:00	18:20	0:20	OS1D	Reluctance Machines 1	OS1D-6	C000694	Optimization of SRG Comprehensive Performance Based on Two-step Commutation
29	Oral	November 27	Room E	16:20-18:20	16:20	16:40	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-1	C000478	Influence of Ratio of Outer Diameter and Axial Length on Torque density in Axial Wound Field Flux Switching Motor with Segmental Rotors

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No	Туре	Date	Room	Time	Start Time	Finish Time	Duration	Session ID	Session Title	Presentation ID	Submission no	Paper Title
30	Oral	November 27	Room E	16:20-18:20	16:40	17:00	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-2	C000825	Analysis of PM Volume Reduction Methods for Hybrid Excitation Switched Flux Machines
31	Oral	November 27	Room E	16:20-18:20	17:00	17:20	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-3	C000136	Axial-Gap Type Adjustable Field Permanent Magnet Synchronous Motor Using Coil-End and Zero-Sequence Current
32	Oral	November 27	Room E	16:20-18:20	17:20	17:40	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-4	C000610	A Study on Performance Improvement via Mag- netic Saturation in a 12-Slot 10-Pole Concen- trated-Winding Permanent-Magnet Motor
33	Oral	November 27	Room E	16:20-18:20	17:40	18:00	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-5	C000757	Proposal of Variable Magnet Vernier Motor for High Efficiency in Wide Speed Range
34	Oral	November 27	Room E	16:20-18:20	18:00	18:20	0:20	OS1E	Flux Switching & Variable Flux Machines 1	OS1E-6	C000151	Design and Analysis of Variable Flux PM Machine for Extending Speed Region to Improve the Drive Cycle Efficiency
35	Oral	November 27	Room F	16:20-18:20	16:20	16:40	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-1	C000555	Harmonic Current Suppression Scheme for Dual Three-Phase PMSM Based on Harmonic Subspace Phase-Shifting Operation
36	Oral	November 27	Room F	16:20-18:20	16:40	17:00	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-2	C000748	DSOGI Based Rotor Position Estimation for DTP-PMSM Considering DC Bias
37	Oral	November 27	Room F	16:20-18:20	17:00	17:20	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-3	C000497	Data-Driven based Model-Free MPC for DTP-PMSM with Optimized Space Vector
38	Oral	November 27	Room F	16:20-18:20	17:20	17:40	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-4	C000898	High Precision Model Predictive Current Control of Dual Three-Phase Permanent Magnet Synchronous Motor
39	Oral	November 27	Room F	16:20-18:20	17:40	18:00	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-5	C000325	A Radial Force Mode Control in IPMSM Using Multi-phase Motor
40	Oral	November 27	Room F	16:20-18:20	18:00	18:20	0:20	OS1F	Multi-winding/Multi-phase Machine Control	OS1F-6	C000902	Online Capacitor Monitoring Strategy In 3L-NPC Inverter Driven Open Winding Multiphase Drives
41	Oral	November 27	Room G	16:20-18:00	16:20	16:45	0:25	SS1	Special Session 1: Bearingless Motos and Drives	SS1-1	C000799	Design, Modelling and Performance Evaluation of a Single-Phase Passively Levitated Self- Bearing Machine
42	Oral	November 27	Room G	16:20-18:00	16:45	17:10	0:25	SS1	Special Session 1: Bearingless Motos and Drives	SS1-2	C000911	Development of a Bearingless PM Motor with Axial Magnetic Suspension Using Zero- Sequence Current
43	Oral	November 27	Room G	16:20-18:00	17:10	17:35	0:25	SS1	Special Session 1: Bearingless Motos and Drives	SS1-3	C000916	Decoupling Force and Torque Generation in Bearingless Motors with Toroidal Windings
44	Oral	November 27	Room G	16:20-18:00	17:35	18:00	0:25	SS1	Special Session 1: Bearingless Motos and Drives	SS1-4	C000919	Comparison of High Pole Number Bearingless Motors with Irregular Distribution of Stator Slots
45	Oral	November 27	Room H	16:20-18:20	16:20	16:40	0:20	OS1H	Induction Motor Control and Drives	OS1H-1	C000400	Predictive Controller Based on Indirect Vector Control for Induction Motor in Electric Vehicle
46	Oral	November 27	Room H	16:20-18:20	16:40	17:00	0:20	OS1H	Induction Motor Control and Drives	OS1H-2	C000726	An Improved Torque Ripple Minimization Pulsewidth Modulation for Induction Motors Under Low Carrier Ratio
47	Oral	November 27	Room H	16:20-18:20	17:00	17:20	0:20	OS1H	Induction Motor Control and Drives	OS1H-3	C000061	Speed Sensor-less Control of Induction Machines in Low-speed Region Based on the Gain- Scheduled Adaptive Flux Observer and Frequency Control
48	Oral	November 27	Room H	16:20-18:20	17:20	17:40	0:20	OS1H	Induction Motor Control and Drives	OS1H-4	C000580	Study on predictive control strategy of pumped- storage DFIM with dual-objective constraint model under grid voltage imbalance condition
49	Oral	November 27	Room H	16:20-18:20	17:40	18:00	0:20	OS1H	Induction Motor Control and Drives	OS1H-5	C000040	Design of an Induction Machine with an Additional Asymmetrical Rotor Winding Providing a Rotor-Fixed Anisotropy for Self-Sensing Control
50	Oral	November 27	Room H	16:20-18:20	18:00	18:20	0:20	OS1H	Induction Motor Control and Drives	OS1H-6	C000412	Real-time Extraction for Stator Interturn Fault Features in Induction Motor Drives using Tracking Filters
51	Oral	November 27	Room I	16:20-18:20	16:20	16:40	0:20	OS1I	PM Motor Control 1	OS1I-1	C000742	Seamless Switch of Control Mode Over Current Vector Control and Voltage Phase Control in IPMSM
52	Oral	November 27	Room I	16:20-18:20	16:40	17:00	0:20	OS1I	PM Motor Control 1	OS1I-2	C000693	Voltage overshoot mitigation for PMSM voltage closed-loop field-weakening control based on a low-pass feedforward compensator
53	Oral	November 27	Room I	16:20-18:20	17:00	17:20	0:20	OS1I	PM Motor Control 1	OS1I-3	C000140	Torque derivative value manipulated type torque feedback control system for PMSM
54	Oral	November 27	Room I	16:20-18:20	17:20	17:40	0:20	OS1I	PM Motor Control 1	OS1I-4	C000735	Active Disturbance Rejection Control - Based on Delayed Signal Cancellation for Current Harmonics Reduction in Permanent Magnet Synchronous Motors Drives
55	Oral	November 27	Room I	16:20-18:20	17:40	18:00	0:20	OS1I	PM Motor Control 1	OS1I-5	C000844	Current Tracking for PMSMs Using Discrete Time Delay Control with Estimation Error Compensation
56	Oral	November 27	Room I	16:20-18:20	18:00	18:20	0:20	OS1I	PM Motor Control 1	OS1I-6	C000872	Ultra-Local Model-Free Predictive Control with Switching Strategy of PMSMs for Two- Phase Stationary Current
57	Oral	November 27	Room J	16:20-18:20	16:20	16:40	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-1	C000071	Towards Sustainable Mobility: Optimal Flux Control of Drive Cycles for Variable Flux Motors via Deep Reinforcement Learning
58	Oral	November 27	Room J	16:20-18:20	16:40	17:00	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-2	C000091	Speed – Torque Range Expansion of In-Wheel Axial-Flux SR Motor for Compact EV

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59	Oral	November 27	Room J	16:20-18:20	17:00	17:20	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-3	C000601	Characteristics of Switched Reluctance Motor using Operating Area Expandable Drive Circuit in Unexpanded Operating Area
60	Oral	November 27	Room J	16:20-18:20	17:20	17:40	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-4	C000141	An Online Torque Sharing Function with Torque Reference Self-Adjusting Method for Switched Reluctance Machines
61	Oral	November 27	Room J	16:20-18:20	17:40	18:00	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-5	C000316	Investigation on The Maximum Efficient Current Waveform of SRM Considering Torque Ripple Reduction
62	Oral	November 27	Room J	16:20-18:20	18:00	18:20	0:20	OS1J	Switched Reluctance Motor Control and Drives	OS1J-6	C000677	Loss Reduction in V/f Control for Switched Reluctance Motor Driven by Single-Pulse Voltage
63	Oral	November 27	Room K	16:20-18:20	16:20	16:40	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-1	C000038	A High Gain Common Ground Inverter without Electrolytic Capacitors
64	Oral	November 27	Room K	16:20-18:20	16:40	17:00	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-2	C000215	A Minimum Backflow Power with Optimal Current Stress Method of Single-Stage DAB Microinverter
65	Oral	November 27	Room K	16:20-18:20	17:00	17:20	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-3	C000506	A Current-Limiting Scheme with Adjustable Virtual Impedance for Three-Phase Four-Wire Grid Forming Inverters
66	Oral	November 27	Room K	16:20-18:20	17:20	17:40	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-4	C000759	A 36-pulse Thyristor Hydrogen Converter Based on a Nine-phase Phase-shifting Transformer
67	Oral	November 27	Room K	16:20-18:20	17:40	18:00	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-5	C000808	Energy Management Strategy of Fuel Cell Management System for Flooding Condition with Distributed Supercapacitors storage element
68	Oral	November 27	Room K	16:20-18:20	18:00	18:20	0:20	OS1K	Power Converters of Renewable Energy Systems 1	OS1K-6	C000055	A Proposal of Permanent Magnet Transverse Flux Generator for Large Wind Turbine Generation System
69	Oral	November 27	Room L	16:20-18:20	16:20	16:40	0:20	OS1L	Power Converters of Motor Drives	OS1L-1	C000537	Space Vector Modulation with Flexible Switching Pause Period Function for Three-Phase PMSM Drive Inverters
70	Oral	November 27	Room L	16:20-18:20	16:40	17:00	0:20	OS1L	Power Converters of Motor Drives	OS1L-2	C000541	High-Power Density Three-Phase Inverter with 3D Circuit Structure Using Liquid Immersion Cooling
71	Oral	November 27	Room L	16:20-18:20	17:00	17:20	0:20	OS1L	Power Converters of Motor Drives	OS1L-3	C000685	Prototype Design and Testing of a Novel Unidirectional Back-to-Back T-Type Three-Level Converter for High Efficiency Applications
72	Oral	November 27	Room L	16:20-18:20	17:20	17:40	0:20	OS1L	Power Converters of Motor Drives	OS1L-4	C000796	Design and Comparison of Multilevel Energy Storage Converter Topologies for High Power Motor Drive Applications
73	Oral	November 27	Room L	16:20-18:20	17:40	18:00	0:20	OS1L	Power Converters of Motor Drives	OS1L-5	C000879	Wide Frequency Range Second Harmonic Suppression in Cascaded H-Bridge Energy Storage Converters Using a Disturbance Observer
74	Oral	November 27	Room L	16:20-18:20	18:00	18:20	0:20	OS1L	Power Converters of Motor Drives	OS1L-6	C000120	Application of GaN E-HEMT to Reaction Wheel Motor Drive
75	Oral	November 28	Room A	9:30-11:35	9:30	9:55	0:25	OGS1	Organized Session 1: Rotating Machines for Traction and I	OGS1-1	C000907	Motor initiatives aimed at reduction of Rare-earth usage
76	Oral	November 28	Room A	9:30-11:35	9:55	10:20	0:25	OGS1	Organized Session 1: Rotating Machines for Traction and I	OGS1-2	C000900	Development of High Power-Density Motors for Electric Axles using Nd-Based Bonded Magnets
77	Oral	November 28	Room A	9:30-11:35	10:20	10:45	0:25	OGS1	Organized Session 1: Rotating Machines for Traction and I	OGS1-3	C000888	Integration of Motor Drive and Charger System with Two-phase Motor and H-Bridge Inverter for Electric Vehicle
78	Oral	November 28	Room A	9:30-11:35	10:45	11:10	0:25	OGS1	Organized Session 1: Rotating Machines for Traction and I	OGS1-4	C000908	Increasing the Power Density of In-Wheel Motor using Direct-Drive Technology
79	Oral	November 28	Room A	9:30-11:35	11:10	11:35	0:25	OGS1	Organized Session 1: Rotating Machines for Traction and I	OGS1-5	C000854	Development of a Megawatt-Class Engine Embedded Electric Machine for Aircraft Electrification
80	Oral	November 28	Room B	9:30-11:50	9:30	9:50	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-1	C000633	The Parameter Sensitivity Analysis of Linear Permanent Magnet Assisted Synchronous Reluctance Motor
81	Oral	November 28	Room B	9:30-11:50	9:50	10:10	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-2	C000823	Maximizing Thrust Force and Reducing Eddy Current Loss in Arc Linear Servo Motors Using 3D FE Analysis of Partial Magnet Segmentation
82	Oral	November 28	Room B	9:30-11:50	10:10	10:30	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-3	C000488	Effect of Primary Iron Core on Performance Characteristics of Linear Switched Reluctance Motor with High-temperature Superconducting Excitation Windings
83	Oral	November 28	Room B	9:30-11:50	10:30	10:50	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-4	C000732	Systemic Stability Evaluation of a Miniature Maglev Drive System for a Pediatric Left Ventricular Assist Device
84	Oral	November 28	Room B	9:30-11:50	10:50	11:10	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-5	C000817	Design Method and Systemic Robustness Evaluation for the Magnetically Levitated Drive System of a Hemocompatibility Assessment Platform
85	Oral	November 28	Room B	9:30-11:50	11:10	11:30	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-6	C000191	Additive Manufacturing Overlapping Winding for Enhanced Performance of a Coreless Permanent Magnet Synchronous Linear Motor
86	Oral	November 28	Room B	9:30-11:50	11:30	11:50	0:20	OS2B	Linear Drives and Magnetic Levitations 1	OS2B-7	C000010	Research on the Characteristics of Multi-Mover Independent Coil Permanent Magnet Linear Synchronous Motor
87	Oral	November 28	Room C	9:30-11:50	9:30	9:50	0:20	OS2C	Permanent Magnet Machines 2	OS2C-1	C000889	Optimal Design of Fractional Slot Number Using Response Surface Method on the Cogging Torque and Unbalanced Magnetic Pull Reduction in Permanent Magnet Machine

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88	Oral	November 28	Room C	9:30-11:50	9:50	10:10	0:20	OS2C	Permanent Magnet Machines 2	OS2C-2	C000561	Design and Analysis of a Hybrid Excitation Synchronous Generator with Radial Additional Air- Gaps
89	Oral	November 28	Room C	9:30-11:50	10:10	10:30	0:20	OS2C	Permanent Magnet Machines 2	OS2C-3	C000813	Achieving Magnetic Force and Cogging Torque Reduction in a Permanent Magnet Generator with Concentrated Slot Technique and Pole Arc Optimization at Magnet Edge
90	Oral	November 28	Room C	9:30-11:50	10:30	10:50	0:20	OS2C	Permanent Magnet Machines 2	OS2C-4	C000014	An Optimized Boundary to Characterize the Relationship between Training Data Quantity and Neural Network Accuracy in Describing Variable Parameters of PMSMs
91	Oral	November 28	Room C	9:30-11:50	10:50	11:10	0:20	OS2C	Permanent Magnet Machines 2	OS2C-5	C000396	Design and optimization of Magnetizer for Axial Flux Permanent Magnet Motor with Halbach Array
92	Oral	November 28	Room C	9:30-11:50	11:10	11:30	0:20	OS2C	Permanent Magnet Machines 2	OS2C-6	C000096	Reconstruction Method of Stator Magnetomotive Force of High-Speed Fault- Tolerant Permanent Magnet Synchronous Motor with Single Winding Independent Control Structure
93	Oral	November 28	Room C	9:30-11:50	11:30	11:50	0:20	OS2C	Permanent Magnet Machines 2	OS2C-7	C000348	Fast Diagnosis of Faults with One-Phase High- Resistance Characteristics in FPPMSM
94	Oral	November 28	Room D	9:30-11:50	9:30	9:50	0:20	OS2D	Synchronous Machines 1	OS2D-1	C000487	Validation of the Analytical Prediction of the Damper Winding Pole-to-Pole Impedance in Hydro Generators
95	Oral	November 28	Room D	9:30-11:50	9:50	10:10	0:20	OS2D	Synchronous Machines 1	OS2D-2	C000568	Digitalization of excitation control circuit for Self-starting salient-pole synchronous motor
96	Oral	November 28	Room D	9:30-11:50	10:10	10:30	0:20	OS2D	Synchronous Machines 1	OS2D-3	C000684	Shaft Voltage Reduction Technique by Layered-Shield of Wound Field Synchronous Motor
97	Oral	November 28	Room D	9:30-11:50	10:30	10:50	0:20	OS2D	Synchronous Machines 1	OS2D-4	C000840	Temperature Calculation Method for Transposed Armature Windings and its Verification through Direct Measurement of Strand Temperatures
98	Oral	November 28	Room D	9:30-11:50	10:50	11:10	0:20	OS2D	Synchronous Machines 1	OS2D-5	C000867	Secondary-Fault Diagnosis of a Rotating Rectifier in a Three-Stage Starter-Generator based on the Idle Winding Terminal Voltage
99	Oral	November 28	Room D	9:30-11:50	11:10	11:30	0:20	OS2D	Synchronous Machines 1	OS2D-6	C000870	Static Testing System for Electromagnetic Torque Characteristics of Synchronous Motors
100	Oral	November 28	Room D	9:30-11:50	11:30	11:50	0:20	OS2D	Synchronous Machines 1	OS2D-7	C000826	Carbon Emission Evaluation and Comparison for Different Electric Machines
101	Oral	November 28	Room E	9:30-11:50	9:30	9:50	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-1	C000490	Fast Calculation of Proximity Loss Induced by Harmonic Current in Electrical Machines Using Magnetic Equivalent Circuit
102	Oral	November 28	Room E	9:30-11:50	9:50	10:10	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-2	C000801	Rotational Magnetic Field Calculation of Electrical Motors by Incorporating a Modified Anisotropic Vector Hysteresis Model
103	Oral	November 28	Room E	9:30-11:50	10:10	10:30	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-3	C000019	Study on Torque Ripple Reduction of Asymmetric Flux Barrier using Topology Optimization and Frozen Permeability Method
104	Oral	November 28	Room E	9:30-11:50	10:30	10:50	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-4	C000822	Theoretical Assessment of Electrical Steel Magnetic Components During PWM-Type Conversion: A Comparison Between Two Hysteresis Models.
105	Oral	November 28	Room E	9:30-11:50	10:50	11:10	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-5	C000553	Lumped Parameter Thermal Network Modeling and Analyzing for a 15 kW, 120000 rpm High-Speed Cage Solid Rotor Induction Motor
106	Oral	November 28	Room E	9:30-11:50	11:10	11:30	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-6	C000702	Modelling for PWM Carrier Loss Evaluation in Claw-pole Machine using MATLAB/Simulink
107	Oral	November 28	Room E	9:30-11:50	11:30	11:50	0:20	OS2E	Numerical Analysis and Modeling 1	OS2E-7	C000138	Analytical Calculation of Cogging Torque Considering Core Reluctance by Using Equivalent Field Winding Model
108	Oral	November 28	Room F	9:30-11:50	9:30	9:50	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-1	C000049	Precise Vibration Measurement with Mechanical Load Isolation for Sub-Fractional Horsepower Motors
109	Oral	November 28	Room F	9:30-11:50	9:50	10:10	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-2	C000156	Temperature Impact on Insulation Lifetime During Electrical Endurance Tests
110	Oral	November 28	Room F	9:30-11:50	10:10	10:30	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-3	C000339	Compensation of Radial Mode 0 Vibration of an Electrically Excited Synchronous Machine using Harmonic Field Current Injection
111	Oral	November 28	Room F	9:30-11:50	10:30	10:50	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-4	C000365	On the use of Machine Learning to improve the analytical NVH predictions of electric machines
112	Oral	November 28	Room F	9:30-11:50	10:50	11:10	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-5	C000418	A Sparsity-Driven Method to Iteratively Extract Motor Fault Signatures in Varying-Speed Operations
113	Oral	November 28	Room F	9:30-11:50	11:10	11:30	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-6	C000626	Determination of the Equivalent Mechanical Properties of the Stator Core for Vibration Analysis in Hydro Generators
114	Oral	November 28	Room F	9:30-11:50	11:30	11:50	0:20	OS2F	Noise, Vibration and Reliability of Electric Machines 1	OS2F-7	C000904	Analysis and Suppression of Synchronous Reluctance Motors with Mirror Asymmetric Rotors
115	Oral	November 28	Room G	9:30-11:50	9:30	9:50	0:20	OS2G	PM Motor Control 2	OS2G-1	C000008	A dual internal mode decoupling control strategy for permanent magnet synchronous motor drives fed by the current source inverter
116	Oral	November 28	Room G	9:30-11:50	9:50	10:10	0:20	OS2G	PM Motor Control 2	OS2G-2	C000465	Current Source Inverter Drive System with Equivalent DC-Machine Control Characteristics

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117	Oral	November 28	Room G	9:30-11:50	10:10	10:30	0:20	OS2G	PM Motor Control 2	OS2G-3	C000195	Torque Synchronous Control for Dual-PMSM Contra-Rotating Propulsion System Based on Parameter Compensation
118	Oral	November 28	Room G	9:30-11:50	10:30	10:50	0:20	OS2G	PM Motor Control 2	OS2G-4	C000670	Hybrid Frequency and Power Dual-Converter for Harmonics Suppression of Open-End Winding High-Speed PMSM
119	Oral	November 28	Room G	9:30-11:50	10:50	11:10	0:20	OS2G	PM Motor Control 2	OS2G-5	C000124	Common Mode Voltage Elimination and Conducted EMI Reduction for Two-unit PMSM
120	Oral	November 28	Room G	9:30-11:50	11:10	11:30	0:20	OS2G	PM Motor Control 2	OS2G-6	C000177	Analysis of High-Frequency Harmonics of The Common Mode Voltage Under AZSPWM1
121	Oral	November 28	Room G	9:30-11:50	11:30	11:50	0:20	OS2G	PM Motor Control 2	OS2G-7	C000255	Control Strategy Considering Angle Difference of PM Synchronous Motor with an Integrated Common-Mode Voltage Filter
122	Oral	November 28	Room H	9:30-11:50	9:30	9:50	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-1	C000402	An Active Disturbance Rejection Control Strategy for the HVDC Generation System of More Electric Aircraft
123	Oral	November 28	Room H	9:30-11:50	9:50	10:10	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-2	C000544	A Starting Control Scheme for Dual Three- Phase Three-Stage Brushless Synchronous Starter/Generator Based on VSD Conversion
124	Oral	November 28	Room H	9:30-11:50	10:10	10:30	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-3	C000572	Parameter-independent Back Electromotive Force Information Estimation Method of the Main Exciter of the Brushless Synchronous Starter Generator
125	Oral	November 28	Room H	9:30-11:50	10:30	10:50	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-4	C000609	A Novel Field Current Estimation Method of the Brushless Synchronous Starter/generator
126	Oral	November 28	Room H	9:30-11:50	10:50	11:10	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-5	C000603	Q-axis Current-based Excitation Current Calculation Method for Torque Ripple Suppression of Hybrid Excitation Machine
127	Oral	November 28	Room H	9:30-11:50	11:10	11:30	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-6	C000587	Suspension Control for Bearingless Doubly Salient Electromagnetic Motor Considering Magnetic Saturation Based on Back Propagation Neural Network
128	Oral	November 28	Room H	9:30-11:50	11:30	11:50	0:20	OS2H	Synchronous Machine Control and Drives 1	OS2H-7	C000760	Small-Signal Modeling and Impedance Analysis of Doubly Salient Electrical-Magnetic Generator Considering Saturation
129	Oral	November 28	Room I	9:30-11:50	9:30	9:50	0:20	OS2I	Sensorless Control 1	OS2I-1	C000190	Discrete Variable Gain Second-Order Sliding Mode Observer Design for Position-Sensorless Control of Permanent Magnet Synchronous
130	Oral	November 28	Room I	9:30-11:50	9:50	10:10	0:20	OS2I	Sensorless Control 1	OS2I-2	C000849	An Improved Speed Observer Based On Current Prediction Compensation for PMSM Sensorless Control
131	Oral	November 28	Room I	9:30-11:50	10:10	10:30	0:20	OS2I	Sensorless Control 1	OS2I-3	C000873	Improvement of Sensorless Rotor Angle Estimation using Zero-sequence Voltage Measurement
132	Oral	November 28	Room I	9:30-11:50	10:30	10:50	0:20	OS2I	Sensorless Control 1	OS2I-4	C000193	Dynamic Position Estimator for a PMSM using Regular Current Sampling and Numerical Optimisation
133	Oral	November 28	Room I	9:30-11:50	10:50	11:10	0:20	OS2I	Sensorless Control 1	OS2I-5	C000596	An Improved Speed Estimation Method for PMSM Using Speed Correction
134	Oral	November 28	Room I	9:30-11:50	11:10	11:30	0:20	OS2I	Sensorless Control 1	OS2I-6	C000618	Double ESO aided Nonlinear Flux Observer for Sensorless Control of PMSM
135	Oral	November 28	Room I	9:30-11:50	11:30	11:50	0:20	OS2I	Sensorless Control 1	OS2I-7	C000206	Sensorless Control Strategy for Permanent Magnet Synchronous Motors Based on Enhanced SOGI- FLL with Limit Cycle Oscillator
136	Oral	November 28	Room J	9:30-11:50	9:30	9:50	0:20	OS2J	Motion Control and Servo Systems	OS2J-1	C000468	Integrated Motor Control with Active Bearings for Speed Regulation with Rotor Imbalance
137	Oral	November 28	Room J	9:30-11:50	9:50	10:10	0:20	OS2J	Motion Control and Servo Systems	OS2J-2	C000862	Iterative Learning Controller Based on Linear Extended State Observer for Six-Degree-of- Freedom Micro-Motion Stage
138	Oral	November 28	Room J	9:30-11:50	10:10	10:30	0:20	OS2J	Motion Control and Servo Systems	OS2J-3	C000401	Speed Control of Separately Excited DC Motor Using Fuzzy Logic Controller
139	Oral	November 28	Room J	9:30-11:50	10:30	10:50	0:20	OS2J	Motion Control and Servo Systems	OS2J-4	C000220	Advanced Task Realization by Robot Fingers Using Mode Quarry Matrix
140	Oral	November 28	Room J	9:30-11:50	10:50	11:10	0:20	OS2J	Motion Control and Servo Systems	OS2J-5	C000280	Motion Analysis of Gravity Compensation Mechanism with Low Inertia Using Parallel Wire Mechanism
141	Oral	November 28	Room J	9:30-11:50	11:10	11:30	0:20	OS2J	Motion Control and Servo Systems	OS2J-6	C000637	A Comparative Study of Vibration Damping Based on Wave Model—Decoupling Reflected Waves from Traveling Waves
142	Oral	November 28	Room J	9:30-11:50	11:30	11:50	0:20	OS2J	Motion Control and Servo Systems	OS2J-7	C000642	Development of a Pneumatic Leader-Follower System with Force Feedback
143	Oral	November 28	Room K	9:30-11:50	9:30	9:50	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-1	C000636	Enhanced Model Predictive Controller Utilizing Kalman Filter for Dual Active Bridge Converter in More Electric Aircraft
144	Oral	November 28	Room K	9:30-11:50	9:50	10:10	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-2	C000455	Non-inverting Buck-Boost (NIBB) Converter Analysis of GaN Half Bridges Operation for 24V Unity Conversion Ratio
145	Oral	November 28	Room K	9:30-11:50	10:10	10:30	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-3	C000727	A Dual Three-Phase <ita>LLC </ita> Resonant Converter With Phase Shedding Strategy for High Power Application

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146	Oral	November 28	Room K	9:30-11:50	10:30	10:50	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-4	C000132	Ripple Current Compensation of DAB Converter with Matching Transformer-Less Series DC Active Filter in DC Distribution Feeder
147	Oral	November 28	Room K	9:30-11:50	10:50	11:10	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-5	C000160	Adaptive Neuron Adjustment for Transient Accuracy Enhancement in FPGA-Based Power Electronics Simulation
148	Oral	November 28	Room K	9:30-11:50	11:10	11:30	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-6	C000359	A Multicellular Converter Topology Allowing for the Scaling of GaN HEMTs to Higher Power Applications
149	Oral	November 28	Room K	9:30-11:50	11:30	11:50	0:20	OS2K	Power Converter 1 (DC-DC)	OS2K-7	C000315	Multiple Output Power Supply Utilizing Multi-Winding Transformers
150	Oral	November 28	Room L	9:30-11:50	9:30	9:50	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-1	C000066	A Seamless Operation of Bidirectional Battery Charger for Electric Vehicles With Power Quality Compensator
151	Oral	November 28	Room L	9:30-11:50	9:50	10:10	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-2	C000022	Adaptive Stabilization of a Three-stage Brushless Generator-Based DC Electrical Power System in More Electric Aircraft
152	Oral	November 28	Room L	9:30-11:50	10:10	10:30	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-3	C000037	Analysis of the Vehicle-grid System Stability Considering Electromagnetic Transient Characteristics of High-Speed Railway Vehicles
153	Oral	November 28	Room L	9:30-11:50	10:30	10:50	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-4	C000081	Quantification of Steady-State Efficiency Maps vs. Time-Stepping Solutions for Drive Cycle Performance Analysis of Induction Motors
154	Oral	November 28	Room L	9:30-11:50	10:50	11:10	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-5	C000147	A Novel Phase-Unit Axial-Modular Permanent Magnet Machine With U-Core Stators for Aerospace Propulsion System
155	Oral	November 28	Room L	9:30-11:50	11:10	11:30	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-6	C000321	Superconducting-based Power Transmission Architecture Design for Hydrogen Hybrid- electric Aircraft
156	Oral	November 28	Room L	9:30-11:50	11:30	11:50	0:20	OS2L	Power Electronics of Mobility Applications	OS2L-7	C000700	Design Study on High Power Density Quasi-Coreless PMSM for Vehicle Traction Drive Rotating at 50,000r/min as the Maximum Speed
157	Oral	November 28	Room A	14:30-16:10	14:30	14:55	0:25	OGS2	Organized Session 2: High Speed Motors and Drives	OGS2-1	C000476	Adaptive Linear Neuron-based Active Disturbance Rejection Control System for Current Harmonics Suppression of PMSM Drives
158	Oral	November 28	Room A	14:30-16:10	14:55	15:20	0:25	OGS2	Organized Session 2: High Speed Motors and Drives	OGS2-2	C000567	MW-class electric propulsion : Geared or Direct Drive?
159	Oral	November 28	Room A	14:30-16:10	15:20	15:45	0:25	OGS2	Organized Session 2: High Speed Motors and Drives	OGS2-3	C000917	Evaluation of AC Copper Loss in High-Speed & High-Power Electric Machines
160	Oral	November 28	Room A	14:30-16:10	15:45	16:10	0:25	OGS2	Organized Session 2: High Speed Motors and Drives	OGS2-4	C000918	Impact of Current Sensor System Dynamics on Current Measurements and Novel Compensation Scheme on dq-Reference Frame
161	Oral	November 28	Room B	14:30-16:30	14:30	14:50	0:20	OS3B	Bearingless Machine 1	OS3B-1	C000052	Homopolar Bearingless slice motor with single- phase suspension windings
162	Oral	November 28	Room B	14:30-16:30	14:50	15:10	0:20	OS3B	Bearingless Machine 1	OS3B-2	C000386	Combined Winding Design for Improving Suspension Force Characteristics of Bearingless Motors
163	Oral	November 28	Room B	14:30-16:30	15:10	15:30	0:20	OS3B	Bearingless Machine 1	OS3B-3	C000505	Five-Degree-of-Freedom Active-Suspended Axial Gap Self-Bearing PMSM with Double Inner Stator
164	Oral	November 28	Room B	14:30-16:30	15:30	15:50	0:20	OS3B	Bearingless Machine 1	OS3B-4	C000691	Proposal of 2-DOF Actively Controlled Consequent-Pole-Type Bearingless Single-Phase Motor Using Zero-Sequence Current
165	Oral	November 28	Room B	14:30-16:30	15:50	16:10	0:20	OS3B	Bearingless Machine 1	OS3B-5	C000086	Rotor Design Study for Exterior Rotor Bearingless Permanent Magnet Machines
166	Oral	November 28	Room B	14:30-16:30	16:10	16:30	0:20	OS3B	Bearingless Machine 1	OS3B-6	C000116	Development of Asymmetrical Four-Phase Bearingless Motor with Unequal-Tooth-Pitch Stator
167	Oral	November 28	Room C	14:30-16:30	14:30	14:50	0:20	OS3C	Multiphase Machines	OS3C-1	C000073	Operation Principle of a Novel Coaxial Triple-DOF Motor
168	Oral	November 28	Room C	14:30-16:30	14:50	15:10	0:20	OS3C	Multiphase Machines	OS3C-2	C000230	Minimization copper loss Full range for single- phase open-circuit fault tolerant control in five- phase SPMSM with non-sinusoidal back EMF
169	Oral	November 28	Room C	14:30-16:30	15:10	15:30	0:20	OS3C	Multiphase Machines	OS3C-3	C000303	Five-Phase PMSM Fault-Diagnostic Strategy Based on Symmetrical Component Method for Weak Inter-Turn Short-Circuit Fault
170	Oral	November 28	Room C	14:30-16:30	15:30	15:50	0:20	OS3C	Multiphase Machines	OS3C-4	C000463	Experimental comparison of a three- and five- phase squirrel cage induction machine
171	Oral	November 28	Room C	14:30-16:30	15:50	16:10	0:20	OS3C	Multiphase Machines	OS3C-5	C000729	Comparison of Electromagnetic and Vibration Performances of Dual Three-Phase and Multiphase SPM Motors
172	Oral	November 28	Room C	14:30-16:30	16:10	16:30	0:20	OS3C	Multiphase Machines	OS3C-6	C000502	Reduction of Carrier Harmonic Iron Loss of Phase-Shift Windings Dual Three-Phase Motors by Phase Current-Shift Control
173	Oral	November 28	Room D	14:30-16:30	14:30	14:50	0:20	OS3D	Flux-Modulated Machines	OS3D-1	C000204	Torque-to-Weight Ratio Improvement of Large-Scale Magnetic Gears for Offshore Wind Power Generation
174	Oral	November 28	Room D	14:30-16:30	14:50	15:10	0:20	OS3D	Flux-Modulated Machines	OS3D-2	C000415	Frequency Response Analysis of Magnetic Coupling and Magnetic Gear

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175	Oral	November 28	Room D	14:30-16:30	15:10	15:30	0:20	OS3D	Flux-Modulated Machines	OS3D-3	C000443	Design and Analysis of Magnetic Gear for Advanced Air mobilities
176	Oral	November 28	Room D	14:30-16:30	15:30	15:50	0:20	OS3D	Flux-Modulated Machines	OS3D-4	C000689	Design and Optimization of High Torque Permanent Magnet Vernier Machines with Fault Tolerance
177	Oral	November 28	Room D	14:30-16:30	15:50	16:10	0:20	OS3D	Flux-Modulated Machines	OS3D-5	C000249	A Novel Efficient and High-Capacity Permanent Magnet Vernier Machine for Urban Intelligent Wind Power Systems
178	Oral	November 28	Room D	14:30-16:30	16:10	16:30	0:20	OS3D	Flux-Modulated Machines	OS3D-6	C000294	High-Torque Rotor Structure with Flux Collection Iron Core in Small Spoke Array Permanent Magnet Vernier Motor
179	Oral	November 28	Room E	14:30-16:30	14:30	14:50	0:20	OS3E	PM Motor Control 3	OS3E-1	C000205	Optimized Full-Speed Range Current Trajectory Control for Permanent Magnet Synchronous Motor System
180	Oral	November 28	Room E	14:30-16:30	14:50	15:10	0:20	OS3E	PM Motor Control 3	OS3E-2	C000576	Efficiency Optimization Control of Surface Permanent Magnet Synchronous Motor Based on Virtual Sinusoidal Signal Injection
181	Oral	November 28	Room E	14:30-16:30	15:10	15:30	0:20	OS3E	PM Motor Control 3	OS3E-3	C000905	An MTPA Control Strategy for IPMSM Based on Virtual Signal Injection Considering the Inverter Nonlinearity
182	Oral	November 28	Room E	14:30-16:30	15:30	15:50	0:20	OS3E	PM Motor Control 3	OS3E-4	C000893	A Reference Flux Calculation Method Using Local Search Algorithm for Maximum Efficiency Operation in Direct Torque Controlled IPMSM Drives
183	Oral	November 28	Room E	14:30-16:30	15:50	16:10	0:20	OS3E	PM Motor Control 3	OS3E-5	C000199	Super-twisting Algorithm Sliding Mode Observer-based Multi-vector Model-free Predictive Control Method for PMSM
184	Oral	November 28	Room E	14:30-16:30	16:10	16:30	0:20	OS3E	PM Motor Control 3	OS3E-6	C000032	A Current Observer for Interior Permanent- Magnet Synchronous Motor with Single DC- Link Current Sensor
185	Oral	November 28	Room F	14:30-16:30	14:30	14:50	0:20	OS3F	Sensorless Control 2	OS3F-1	C000238	Position Sensorless Control of CHB Converter Fed Three-Phase PMSM Drives Using Collaborative High-Frequency Square-Wave Voltage Injection
186	Oral	November 28	Room F	14:30-16:30	14:50	15:10	0:20	OS3F	Sensorless Control 2	OS3F-2	C000816	Sensorless Noise Reduction Strategy for Permanent Magnet Synchronous Motor Based on Random High-Frequency Sinusoidal Injection
187	Oral	November 28	Room F	14:30-16:30	15:10	15:30	0:20	OS3F	Sensorless Control 2	OS3F-3	C000439	Extraction of the Sampled High-Frequency Current Trajectory with a Novel Synchronous Minor Sampling Process in IPMSM using PWM Carrier-Synchronized Voltage Injections
188	Oral	November 28	Room F	14:30-16:30	15:30	15:50	0:20	OS3F	Sensorless Control 2	OS3F-4	C000573	Study of Direct Torque Control With Reference Flux Vector Calculation for Position Sensorless IPMSM Drives With High-Frequency Signal Injection
189	Oral	November 28	Room F	14:30-16:30	15:50	16:10	0:20	OS3F	Sensorless Control 2	OS3F-5	C000454	Artificial Intelligence-based Sensorless Control of Non-Sinusoidal Seven-Phase PMSM
190	Oral	November 28	Room F	14:30-16:30	16:10	16:30	0:20	OS3F	Sensorless Control 2	OS3F-6	C000176	A Novel Sensorless Sliding-Mode Control of PMSM with VSI Nonlinearity Compensation
191	Oral	November 28	Room G	14:30-16:10	14:30	14:55	0:25	SS2	Special Session 2: Current Pulse Driven Motor and Its Driving Circuit	SS2-1	C000656	High Pulse Current IGBT Power Module for MRM Drive
192	Oral	November 28	Room G	14:30-16:10	14:55	15:20	0:25	SS2	Special Session 2: Current Pulse Driven Motor and Its Driving Circuit	SS2-2	C000914	A Novel Magnet Reversal Motor (MRM) Driven by High Pulse Current for Copper Loss Reduction
193	Oral	November 28	Room G	14:30-16:10	15:20	15:45	0:25	SS2	Special Session 2: Current Pulse Driven Motor and Its Driving Circuit	SS2-3	C000909	High Pulse and Sinusoidal Current Output Inverter for MRM Drive
194	Oral	November 28	Room G	14:30-16:10	15:45	16:10	0:25	SS2	Special Session 2: Current Pulse Driven Motor and Its Driving Circuit	SS2-4	C000871	Gate Driver IC With Fully Integrated Overcurrent Protection for Driving Magnet Reversal Motor With High Pulse Current
195	Oral	November 28	Room H	14:30-16:30	14:30	14:50	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-1	C000089	A Diagnostic Method for Inter-Turn Short Circuit Faults Based on High Frequency Park Vectors
196	Oral	November 28	Room H	14:30-16:30	14:50	15:10	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-2	C000340	Interturn Short-Circuit Fault Diagnosis Method of Permanent Magnet Synchronous Motor Based on Phase Current Residuals
197	Oral	November 28	Room H	14:30-16:30	15:10	15:30	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-3	C000353	Multireference-Frame Based Model Predictive Fault-Tolerant Control for Dual Three-Phase Permanent Magnet Synchronous Machines
198	Oral	November 28	Room H	14:30-16:30	15:30	15:50	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-4	C000423	Natural Fault-Tolerant Control Strategy of Dual Three-Phase PMSM Drives With a Common Neutral Point Under Open-Circuit Fault
199	Oral	November 28	Room H	14:30-16:30	15:50	16:10	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-5	C000850	A Fault-tolerant Control Strategy for Multiphase Motor Based on MPC Modulation
200	Oral	November 28	Room H	14:30-16:30	16:10	16:30	0:20	OS3H	Fault diagnosis & Fault-tolerant Control	OS3H-6	C000584	An Improved Fault-Tolerant Control for PMSM with Current Sensor Fault
201	Oral	November 28	Room I	14:30-16:30	14:30	14:50	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-1	C000166	A Hybrid Modulation Strategy and Loss Modeling of Si/SiC Seven-Level Converter for Aircraft Electric Propulsion
202	Oral	November 28	Room I	14:30-16:30	14:50	15:10	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-2	C000239	An Improved Si/SiC Hybrid Three-Level ANPC Inverter with Optimized Thermal Distribution- Based Modulation Scheme
203	Oral	November 28	Room I	14:30-16:30	15:10	15:30	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-3	C000251	An Octal-Switch Redundant Submodule for MMC to Tolerate Open-Circuit Faults

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204	Oral	November 28	Room I	14:30-16:30	15:30	15:50	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-4	C000705	A Coupling-Transformerless Voltage-Fed Active EMI Filter for Two-Stage PV Inverters
205	Oral	November 28	Room I	14:30-16:30	15:50	16:10	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-5	C000598	Improvement and Analysis of 3-phase DCLA with Unequally Divided Source Voltage for Actual Implementation
206	Oral	November 28	Room I	14:30-16:30	16:10	16:30	0:20	OS3I	Power Converter 2 (DC-AC)	OS3I-6	C000067	Loss Equalization of Unbalanced Three-phase Inverter by Pulse-voltage-injection Two-phase PWM using Variable Switching Pause Period
207	Oral	November 28	Room J	14:30-16:30	14:30	14:50	0:20	OS3J	Control of Power Converter	OS3J-1	C000313	Experimental Verification of Discontinuous Current Mode for Boost Inverters
208	Oral	November 28	Room J	14:30-16:30	14:50	15:10	0:20	OS3J	Control of Power Converter	OS3J-2	C000363	High-robustness Capacitor Voltage Active Damping based on Model Free Predictive Current Control for ANPC GCI with LCL Filter
209	Oral	November 28	Room J	14:30-16:30	15:10	15:30	0:20	OS3J	Control of Power Converter	OS3J-3	C000775	A New Control method and power response of power compensator with low switching frequency
210	Oral	November 28	Room J	14:30-16:30	15:30	15:50	0:20	OS3J	Control of Power Converter	OS3J-4	C000043	Evaluation of Automatic Adjustment Methods for Voltage Reference to Compensate Dead- time Distortion using Machine Learning
211	Oral	November 28	Room J	14:30-16:30	15:50	16:10	0:20	OS3J	Control of Power Converter	OS3J-5	C000669	A Survey of Lifetime Extension Techniques for High-Reliability Power Electronics
212	Oral	November 28	Room J	14:30-16:30	16:10	16:30	0:20	OS3J	Control of Power Converter	OS3J-6	C000761	Fault diagnosis method of servo motor bearing installation misalignment based on CSFF-CNN
213	Oral	November 28	Room K	14:30-16:30	14:30	14:50	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-1	C000429	Low Frequency AC Transmission for Offshore Wind Power
214	Oral	November 28	Room K	14:30-16:30	14:50	15:10	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-2	C000562	Improved Damping Control Based on Hamiltonian Control Law for Low-carbon Hydrogen Production Systems
215	Oral	November 28	Room K	14:30-16:30	15:10	15:30	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-3	C000736	Sensorless Control Strategy of Remote Area Autonomous PMSG-Based Microgrids for Improving Redundancy
216	Oral	November 28	Room K	14:30-16:30	15:30	15:50	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-4	C000838	Autonomous Passivity Model Predictive Control for Fixed-Time Feedforward Decoupling of DC Microgrids With Constant Power Loads
217	Oral	November 28	Room K	14:30-16:30	15:50	16:10	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-5	C000144	Impact Analysis of the Distribution and Installation Proportions of Grid-Forming and Grid- Following Converters on the Stability of A 100% Renewable Energy System
218	Oral	November 28	Room K	14:30-16:30	16:10	16:30	0:20	OS3K	Power Converters of Renewable Energy Systems 2	OS3K-6	C000211	Power Control Using Sub-Battery for Electric Motorcycle
219	Oral	November 28	Room L	14:30-16:30	14:30	14:50	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-1	C000154	An Online Auto-Tuning Method for PID Controllers Based on Back Propagation Neural Network
220	Oral	November 28	Room L	14:30-16:30	14:50	15:10	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-2	C000256	Evaluation of Feasibility for Optimal Motor Design using Deep Q-Network
221	Oral	November 28	Room L	14:30-16:30	15:10	15:30	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-3	C000281	A Study of Motor Fault Condition Classification Using an Unsupervised Learning- Based Ensemble Model
222	Oral	November 28	Room L	14:30-16:30	15:30	15:50	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-4	C000824	Comparison of Recurrent Neural Networks on Dry-type Transformer Thermal Models under Various Conditions
223	Oral	November 28	Room L	14:30-16:30	15:50	16:10	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-5	C000860	Gear Fault Diagnosis in Geared Motors based on Frequency Adaptation Graph Prototype Network with Limited Data
224	Oral	November 28	Room L	14:30-16:30	16:10	16:30	0:20	OS3L	Al Application for Electric Machine and Drive	OS3L-6	C000092	Heuristic investigation of the required amount of data as part of the scalable data-based diagnostic concept
225	Oral	November 29	Room A	9:30-11:35	9:30	9:55	0:25	OGS3	Organized Session 3: Power Conversion Technology for Multiple Objectives in Motor Drives	OGS3-1	C000901	Buck-Boost Operation by Zero-Sequence Current Control for Negative-Point-Connected Dual Inverter with Variable Voltage Capacitor
226	Oral	November 29	Room A	9:30-11:35	9:55	10:20	0:25	OGS3	Organized Session 3: Power Conversion Technology for Multiple Objectives in Motor Drives	OGS3-2	C000899	Transition and Latest Technology of Power Electronics for Air Conditioners
227	Oral	November 29	Room A	9:30-11:35	10:20	10:45	0:25	OGS3	Organized Session 3: Power Conversion Technology for Multiple Objectives in Motor Drives	OGS3-3	C000887	A Novel Single-Phase AC Power Supplied Dual-Inverter Topology with Integrated Rectifier
228	Oral	November 29	Room A	9:30-11:35	10:45	11:10	0:25	OGS3	Organized Session 3: Power Conversion Technology for Multiple Objectives in Motor Drives	OGS3-4	C000910	Magnet Synchronous Motor Using Negative-Point-Connected Dual Inverter with Variable
229	Oral	November 29	Room A	9:30-11:35	11:10	11:35	0:25	OGS3	Organized Session 3: Power Conversion Technology for Multiple Objectives in Motor Drives	OGS3-5	JIA-to-ICEMS	TBD
230	Oral	November 29	Room B	9:30-11:50	9:30	9:50	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-1	C000152	Evaluation of Support Stiffness of a Permanent Magnet Attractive Force Type Passive Magnetic Bearing
231	Oral	November 29	Room B	9:30-11:50	9:50	10:10	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-2	C000720	Multi-objective Parameter Optimization Design of Radial Magnetic Levitation Bearing
232	Oral	November 29	Room B	9:30-11:50	10:10	10:30	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-3	C000724	A Mixed Sensitivity H ∞ Control Method Based on Active Magnetic Bearing

No	Туре	Date	Room	Time	Start Time	Finish Time	Duration	Session ID	Session Title	Presentation ID	Submission no	Paper Title
233	Oral	November 29	Room B	9:30-11:50	10:30	10:50	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-4	C000798	Topology Optimization of an Alternate Permanent Magnet Electrodynamic Suspension Using a 3-D Hybrid Analytical Model
234	Oral	November 29	Room B	9:30-11:50	10:50	11:10	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-5	C000344	Thrust Analysis of a Reluctance-Based Magnetic Lead Screw with Flux-Concentrating Structure
235	Oral	November 29	Room B	9:30-11:50	11:10	11:30	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-6	C000585	Basic Consideration of Topology Optimization for Eddy Current Dampers
236	Oral	November 29	Room B	9:30-11:50	11:30	11:50	0:20	OS4B	Linear Drives and Magnetic Levitations 2	OS4B-7	C000279	Proposal for Estimation of Modal Damping Ratio in Electromagnetic Bone Conduction Devices
237	Oral	November 29	Room C	9:30-11:50	9:30	9:50	0:20	OS4C	Permanent Magnet Machines 3	OS4C-1	C000134	Structural Study of IPMSMs Achieving Both High Torque and Wide Constant Power Operating Range
238	Oral	November 29	Room C	9:30-11:50	9:50	10:10	0:20	OS4C	Permanent Magnet Machines 3	OS4C-2	C000180	Research on the Optimization of Power Density and Its Influencing Factors of the YASA Motor
239	Oral	November 29	Room C	9:30-11:50	10:10	10:30	0:20	OS4C	Permanent Magnet Machines 3	OS4C-3	C000219	AC Copper Loss Separation and Reduction in IPMSM using Finite Element Analysis
240	Oral	November 29	Room C	9:30-11:50	10:30	10:50	0:20	OS4C	Permanent Magnet Machines 3	OS4C-4	C000224	Design and analysis of Permanent Magnet Synchronous Machine with High Power Density for Aircraft Starter-Generator
241	Oral	November 29	Room C	9:30-11:50	10:50	11:10	0:20	OS4C	Permanent Magnet Machines 3	OS4C-5	C000234	Characterization of a High Torque Density Halbach Motor in UAV Application
242	Oral	November 29	Room C	9:30-11:50	11:10	11:30	0:20	OS4C	Permanent Magnet Machines 3	OS4C-6	C000093	Design and Analysis of In-wheel Flux Reversal Motor for Compact EV
243	Oral	November 29	Room C	9:30-11:50	11:30	11:50	0:20	OS4C	Permanent Magnet Machines 3	OS4C-7	C000591	Multi-Objective Robust Optimization of a Low- Cost and Efficient IPMSM for Battery Electric Vehicle
244	Oral	November 29	Room D	9:30-11:50	9:30	9:50	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-1	C000309	Research on Immersion Evaporative Cooling under Different Pressure Conditions in High power density Motor
245	Oral	November 29	Room D	9:30-11:50	9:50	10:10	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-2	C000495	A Baseline Thermal Model for Liquid-Cooled Multi-Megawatt Scale Direct-Drive Permanent Magnet Wind Turbine Generators
246	Oral	November 29	Room D	9:30-11:50	10:10	10:30	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-3	C000710	Computationally efficient estimation of thermally induced stresses in motorette using numerical homogenization techniques and experimental validation
247	Oral	November 29	Room D	9:30-11:50	10:30	10:50	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-4	C000866	Experimental Investigation of Windage Loss Impacts on Electrical Machine with Oil Jet Cooling
248	Oral	November 29	Room D	9:30-11:50	10:50	11:10	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-5	C000178	Loss Evaluation in a Ductile Cast Iron Frame of a Permanent Magnet Synchronous Motor
249	Oral	November 29	Room D	9:30-11:50	11:10	11:30	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-6	C000462	Evaluation of Inverter Topologies and Switching Frequencies Regarding Harmonic Losses in PMSM
250	Oral	November 29	Room D	9:30-11:50	11:30	11:50	0:20	OS4D	Loss, Thermal and Cooling of Electric Machines	OS4D-7	C000036	Measurement of Magnetic Parameters with Focus on Eddy Current Losses in Permanent Magnets of Electrical Machines Using Flexible Matrix Sensors
251	Oral	November 29	Room E	9:30-11:50	9:30	9:50	0:20	OS4E	Superconducting & Special Machines	OS4E-1	C000188	Superconductive GdBaCuO 3-phase High Speed Outrunner Motor for High Load Cargo Drones
252	Oral	November 29	Room E	9:30-11:50	9:50	10:10	0:20	OS4E	Superconducting & Special Machines	OS4E-2	C000410	Study on AC Loss Reduction in HTS motors for Electrified Aircraft Propulsion
253	Oral	November 29	Room E	9:30-11:50	10:10	10:30	0:20	OS4E	Superconducting & Special Machines	OS4E-3	C000331	Analysis on the characteristics of the decompression cooling system used in the superconducting motor
254	Oral	November 29	Room E	9:30-11:50	10:30	10:50	0:20	OS4E	Superconducting & Special Machines	OS4E-4	C000097	Dynamic Non-Linear Numerical-Analytical Model for Synchronous Homopolar Machines
255	Oral	November 29	Room E	9:30-11:50	10:50	11:10	0:20	OS4E	Superconducting & Special Machines	OS4E-5	C000125	Design and evaluation of a flat PCB based axial flux motor
256	Oral	November 29	Room E	9:30-11:50	11:10	11:30	0:20	OS4E	Superconducting & Special Machines	OS4E-6	C000711	A Double-Feed Magnetic Resonant Coupling Machine with Air-Gap Windings for High Power Density and Efficiency
257	Oral	November 29	Room E	9:30-11:50	11:30	11:50	0:20	OS4E	Superconducting & Special Machines	OS4E-7	C000382	Transmission Torque Characteristics of Strain Wave Gear with 16-poles Magnet
258	Oral	November 29	Room F	9:30-11:50	9:30	9:50	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-1	C000161	Online MTPA Angle Search Method Using Flux Linkage Plane Estimation of SynRM
259	Oral	November 29	Room F	9:30-11:50	9:50	10:10	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-2	C000217	Position Estimation and Parameter Identification of SynRM at Standstill
260	Oral	November 29	Room F	9:30-11:50	10:10	10:30	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-3	C000483	Maximum Torque Per Ampere Control implemented Hardware System for Synchronous Reluctance Motor
261	Oral	November 29	Room F	9:30-11:50	10:30	10:50	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-4	C000258	Voltage Angle Regulated Field Weakening Control Based on Overmodulation Strategy for PMa-SynRM Drives

No	Туре	Date	Room	Time	Start Time	Finish Time	Duration	Session ID	Session Title	Presentation ID	Submission no	Paper Title
262	Oral	November 29	Room F	9:30-11:50	10:50	11:10	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-5	C000865	Dual Inverter Controlled Third Harmonic Current Injection Scheme for an Open-end Winding Brushless Wound Rotor Synchronous Machine
263	Oral	November 29	Room F	9:30-11:50	11:10	11:30	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-6	C000392	Acoustic Noise Reduction in Resolver-based PMSM Servo Drives using NLMS Adaptive Filtering
264	Oral	November 29	Room F	9:30-11:50	11:30	11:50	0:20	OS4F	Synchronous Machine Control and Drives 2	OS4F-7	C000494	Applying partial PAM method suitable for robot motor drive
265	Oral	November 29	Room G	9:30-11:50	9:30	9:50	0:20	OS4G	PM Motor Control 4	OS4G-1	C000295	Implementation and Validation of a LUT-Based Model of an IPMSM Considering Saturation and Spatial Harmonics
266	Oral	November 29	Room G	9:30-11:50	9:50	10:10	0:20	OS4G	PM Motor Control 4	OS4G-2	C000114	Impact of Voltage Modulation Module on Negative Input Impedance and DC-Link Stability in Permanent Magnet Synchronous Motor Drives
267	Oral	November 29	Room G	9:30-11:50	10:10	10:30	0:20	OS4G	PM Motor Control 4	OS4G-3	C000054	Influence of <ita>d</ita> -Axis Current on Torque and Transformer Secondary-side Power in Power Superposition System for Position Sensor of Surface-mounted PMSM
268	Oral	November 29	Room G	9:30-11:50	10:30	10:50	0:20	OS4G	PM Motor Control 4	OS4G-4	C000770	Improvement Performance of FOC for PMSM Based on Reinforcement Learning TD3 Agent Current Controller
269	Oral	November 29	Room G	9:30-11:50	10:50	11:10	0:20	OS4G	PM Motor Control 4	OS4G-5	C000447	Torque Control Characteristics of Simple Controller-Based Direct Torque Control for PMSM Drive System
270	Oral	November 29	Room G	9:30-11:50	11:10	11:30	0:20	OS4G	PM Motor Control 4	OS4G-6	C000471	Modulation Signal Optimized Synchronous PWM
271	Oral	November 29	Room G	9:30-11:50	11:30	11:50	0:20	OS4G	PM Motor Control 4	OS4G-7	C000652	An Accurate Measurement Method for Iron Loss Resistance of Permanent Magnet Synchronous Motor
272	Oral	November 29	Room H	9:30-11:50	9:30	9:50	0:20	OS4H	Sensorless Control 3	OS4H-1	C000683	Torque Ripple Suppression Control in Medium to High-Speed Ranges with Position Sensorless Vector Control
273	Oral	November 29	Room H	9:30-11:50	9:50	10:10	0:20	OS4H	Sensorless Control 3	OS4H-2	C000716	A Mutual Inductance Estimation Based Sensorless Control for IPMSM with Complex- Coefficient Filter in Low-Speed Range
274	Oral	November 29	Room H	9:30-11:50	10:10	10:30	0:20	OS4H	Sensorless Control 3	OS4H-3	C000101	Robust Deadbeat Predictive Current Control for High-speed Synchronous machine Sensorless Drive with Instant Inductance Identification
275	Oral	November 29	Room H	9:30-11:50	10:30	10:50	0:20	OS4H	Sensorless Control 3	OS4H-4	C000287	Sensorless Control for IPM with Adaptive Resistance Estimation Using Flux Norm Correction
276	Oral	November 29	Room H	9:30-11:50	10:50	11:10	0:20	OS4H	Sensorless Control 3	OS4H-5	C000122	Suppression of Velocity Pulsations with Resonant Controllers in Sensorless Vector Control of Permanent Magnet Synchronous Motors
277	Oral	November 29	Room H	9:30-11:50	11:10	11:30	0:20	OS4H	Sensorless Control 3	OS4H-6	C000717	Efficient I-F startup method for refrigeration compressors
278	Oral	November 29	Room H	9:30-11:50	11:30	11:50	0:20	OS4H	Sensorless Control 3	OS4H-7	C000069	Vibration Suppression Method using Disturbance Observer in Sensorless 120-degree Conduction Compressor Motor Drive
279	Oral	November 29	Room I	9:30-11:50	9:30	9:50	0:20	OS4I	Linear Motor Control and Drives	OS4I-1	C000305	Design for Bidirectional Movement of Bendable Tubular Linear Motor
280	Oral	November 29	Room I	9:30-11:50	9:50	10:10	0:20	OS4I	Linear Motor Control and Drives	OS4I-2	C000730	Research on the Influence Mechanism and Stability Control Method of Composite Disturbance on Double-End Power Supply of High Speed Maglev Traction System
281	Oral	November 29	Room I	9:30-11:50	10:10	10:30	0:20	OS4I	Linear Motor Control and Drives	OS4I-3	C000875	A Novel Segment Switching Method for Dual Three-Phase Linear Motors with Stator Segmented Powered
282	Oral	November 29	Room I	9:30-11:50	10:30	10:50	0:20	OS4I	Linear Motor Control and Drives	OS4I-4	C000876	A Smooth Power Supply Switching Method of Segmented Long Primary Linear Motors for High-Speed Applications
283	Oral	November 29	Room I	9:30-11:50	10:50	11:10	0:20	OS4I	Linear Motor Control and Drives	OS4I-5	C000034	Full-Decoupled Two-Degree-of-Freedom Position Controller for PMSLM Based on ADRC
284	Oral	November 29	Room I	9:30-11:50	11:10	11:30	0:20	OS4I	Linear Motor Control and Drives	OS4I-6	C000424	Friction Compensation Method with Iterative Learning Based Bang-Bang Compensator in PMLSM system
285	Oral	November 29	Room I	9:30-11:50	11:30	11:50	0:20	OS4I	Linear Motor Control and Drives	OS4I-7	C000117	Adaptive Feedforward Control Based on Recursive Least Squares Algorithm for the Biaxial Maglev Planar-Motor-Driven Gantry System
286	Oral	November 29	Room J	9:30-11:50	9:30	9:50	0:20	OS4J	Power Converter 3 (WPT)	OS4J-1	C000441	High Distance to Diameter Ratio Wireless Power Trans-fer System
287	Oral	November 29	Room J	9:30-11:50	9:50	10:10	0:20	OS4J	Power Converter 3 (WPT)	OS4J-2	C000661	Analysis of Low-eddy Current WPT Applied in Underground Coal Mines
288	Oral	November 29	Room J	9:30-11:50	10:10	10:30	0:20	OS4J	Power Converter 3 (WPT)	OS4J-3	C000714	A Novel Capacitive Power Transfer System with Embedded Coupler for Rotary Application
289	Oral	November 29	Room J	9:30-11:50	10:30	10:50	0:20	OS4J	Power Converter 3 (WPT)	OS4J-4	C000781	Characteristic analysis of coupling mechanism for wireless power transfer system with transparent window used in coal mine
290	Oral	November 29	Room J	9:30-11:50	10:50	11:10	0:20	OS4J	Power Converter 3 (WPT)	OS4J-5	C000686	WPT Coil Position for Minimizing SOC Fluctuations in Battery-Powered Trains

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No	Туре	Date	Room	Time	Start Time	Finish Time	Duration	Session ID	Session Title	Presentation ID	Submission no	Paper Title
291	Oral	November 29	Room J	9:30-11:50	11:10	11:30	0:20	OS4J	Power Converter 3 (WPT)	OS4J-6	C000851	Coupling Coefficient Estimation Method for SP-Type Wireless Power Transfer System
292	Oral	November 29	Room J	9:30-11:50	11:30	11:50	0:20	OS4J	Power Converter 3 (WPT)	OS4J-7	C000660	Hybrid Closed-Form Modulation Scheme for Three-Phase Dual-Active Bridge with Reduced RMS Current
293	Oral	November 29	Room K	9:30-11:50	9:30	9:50	0:20	OS4K	Power Converter (general)	OS4K-1	C000863	Simulation Platform for GaN-based Three- Phase Voltage Source Inverter Analysis: Switching Frequency and Deadtime
294	Oral	November 29	Room K	9:30-11:50	9:50	10:10	0:20	OS4K	Power Converter (general)	OS4K-2	C000551	Application of Mn-Zn Ferrite to Passive Common-Noise Canceller Placed on Inverter DC Side
295	Oral	November 29	Room K	9:30-11:50	10:10	10:30	0:20	OS4K	Power Converter (general)	OS4K-3	C000569	Passive Cancellation for Reducing Input- and Output-Side Common-Mode Currents in Three- Phase PWM Inverter-Fed Motor Drive Systems
296	Oral	November 29	Room K	9:30-11:50	10:30	10:50	0:20	OS4K	Power Converter (general)	OS4K-4	C000504	Efficient and Compact 400-V, 100-A Solid-State Circuit Breaker Using SiC Devices
297	Oral	November 29	Room K	9:30-11:50	10:50	11:10	0:20	OS4K	Power Converter (general)	OS4K-5	C000355	An Energy-Saving Strategy for Permanent Magnet Synchronous Motors System
298	Oral	November 29	Room K	9:30-11:50	11:10	11:30	0:20	OS4K	Power Converter (general)	OS4K-6	C000026	Improved Sliding Mode Control Method Using a Hyperbolic Function for Battery Charger of PMDs
299	Oral	November 29	Room K	9:30-11:50	11:30	11:50	0:20	OS4K	Power Converter (general)	OS4K-7	C000782	Parallel Grid-Forming Inverters for 100% Inverter-Based Resources RE100 Microgrid - Emphasis on Secondary Control-
300	Oral	November 29	Room L	9:30-11:50	9:30	9:50	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-1	C000514	An Improved Super-Twisting Sliding Mode Controller over Totem-Pole Power Factor Corrector
301	Oral	November 29	Room L	9:30-11:50	9:50	10:10	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-2	C000528	Low Harmonic 24-pulse Rectifier Based on Square-wave Voltage Injection
302	Oral	November 29	Room L	9:30-11:50	10:10	10:30	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-3	C000728	A Synchronous Rectification Strategy Driven by Current and Digital for Three Phase LLC Resonant Converter
303	Oral	November 29	Room L	9:30-11:50	10:30	10:50	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-4	C000814	Simplified Linear Kalman Filter for Sensorless Oriented Control of PWM Rectifiers
304	Oral	November 29	Room L	9:30-11:50	10:50	11:10	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-5	C000012	Fault-Tolerant Strategy of Flying-Capacitor Boost Three Level Converter
305	Oral	November 29	Room L	9:30-11:50	11:10	11:30	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-6	C000698	Evaluation of The Impact of Power Quality on Each Home Appliance
306	Oral	November 29	Room L	9:30-11:50	11:30	11:50	0:20	OS4L	Power Converter 3 (AC-DC)	OS4L-7	C000131	Power Balancing Control of Sub Modules with Battery Units in Single-Phase Grid-Tied MMC Under Unbalanced Generated Power

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No	Туре	Date	Room	Time	Session ID	Session Title	Presentation ID	Order	Submission no	Paper Title
1	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-1	1	C000556	Experimental Investigation on the Influence of a Hollow Rotor Shaft Cooling and Oil Properties on No-Load Losses in Traction Electric Machines
2	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-2	2	C000583	Novel Refrigerant Cooling Method for Traction Motor Thermal Management
3	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-3	3	C000807	Analysis and Desing of IPMSM for Reducing AC Copper Loss in EV Traction Motor
4	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-4	4	C000326	Impact of Leakage Flux on Permanent Magnet Synchronous Machines in Traction Drives Using 2D and 3D Finite Element Analysis Comparative Study
5	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-5	5	C000337	Experimental validation of a prediction method for bearing currents in traction drive systems
6	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-6	6	C000749	Rotor Design Considering Demagnetization Characteristics of Ribless IPMSM for EV Propulsion
7	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-7	7	C000843	Review of High Torque Density Permanent Magnet Machines for Electric Propulsion System
8	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-8	8	C000442	Optimisation of Permanent Magnet Synchronous Motor for Electric Vehicles
9	Poster	November 27	FIT Arena	13:00-14:00	PS1-1	Permanent Magnet Machines 4	PS1-1-9	9	C000369	Optimization Study of Torque in the IPMSM for E-bike Application
10	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-1	1	C000864	Design and Optimization of an Outer-Rotor PMSM for Torque Ripple Minimization
11	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-2	2	C000274	Comparative Analysis of Torque Ripple in IPMSM Topologies using the Frozen Permeability Method
12	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-3	3	C000158	Fault-Tolerant Control Method to Reduce Torque Ripple for Symmetrical Winding Multi-Phase Brushless DC Motor Under Open-Circuit Faults
13	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-4	4	C000039	An Optimization Design for Reducing Cogging Torque in Permanent Magnet Synchronous Motors
14	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-5	5	C000451	Investigation and Analysis of Cogging Torque for Axial Flux Permanent Magnet Machines
15	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-6	6	C000480	Study of Rotor Slotting on Cogging Torque of Spoke-Type Permanent Magnet Machine
16	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-7	7	C000050	Reduction of Axial Magnetic force and Starting Current in Single-Sided Axial-flux Machine with Ring PM Unit and Flux-Weakening Control
17	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-8	8	C000913	Vibration and Noise Analysis and Suppression of High Torque Density Permanent Magnet Motor
18	Poster	November 27	FIT Arena	13:00-14:00	PS1-2	Permanent Magnet Machines 5	PS1-2-9	9	C000706	Unbalanced magnetic radial pull during module open circuit fault in a multi-modular, high voltage PM synchronous direct drive generator for offshore wind
19	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-1	1	C000472	Multi-Objective Optimization of a Novel Permanent Magnet Starter-Generator
20	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-2	2	C000912	Multi-Objective Optimization for a Low-speed High-torque Permanent Magnet Motor
21	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-3	3	C000874	Analytical Modeling and Optimization of Three-Segment Halbach Permanent Magnet Array High Lift Motor
22	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-4	4	C000284	Optimization Design Research of Dual-Airgap High-Torque Permanent Magnet Motor Based on Coevolution Algorithm
23	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-5	5	C000297	Improved IPM Motor Design with Integrated Ribs for Stress Reduction and Weight Optimization
24	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-6	6	C000074	Back EMF Waveform Optimization of Hybrid Less Rare-earth Synchronous Reluctance Motor Using PSO Algorithm
25	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-7	7	C000464	Cost Optimization Method for Less-Rare-Earth Permanent Magnet Synchronous Motor Based on Surrogate Model
26	Poster	November 27	FIT Arena	13:00-14:00	PS1-3	Permanent Magnet Machines 6	PS1-3-8	8	C000589	Design proposal Based on Characteristic Analysis of Permanent Magnet Utilization Ratio in Dual Rotor IPMSM
27	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-1	1	C000064	Magnet Reduction Effect of Split Rotor and Non-Magnetic Wedge in V-shaped Interior Permanent Magnet Motor
28	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-2	2	C000259	Investigation of Angle Displacements in A Novel Dual-Three-Phase Equinumerous-Slot- Pole PMSM
29	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-3	3	C000242	Design and Performance Analysis of a Novel Permanent Magnet Synchronous Motor with Stepped Magnetic Poles

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30	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-4	4	C000350	A Novel Permanent Magnet Synchronous Machines with Improved Magnetic Field Characteristics and Performance Analysis
31	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-5	5	C000644	Design and Analysis of Fractional-slot Concentrated Winding PMSMs with Unequal Tooth Towards Improving Torque Density
32	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-6	6	C000228	A Novel Two Degrees-of-Freedom Rotary- linear Permanent Magnet Machine
33	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-7	7	C000779	Design and Analysis of a Rotor-Coreless Multi-Disk Axial Flux Permanent Magnet Motor with Unaligned Permanent Magnets
34	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-8	8	C000368	Design and Analysis of Permanent Magnet Synchronous Motor Based on Asymmetric Auxiliary Teeth for Rotor Mechanical Position Self-Sensing Technology
35	Poster	November 27	FIT Arena	13:00-14:00	PS1-4	Permanent Magnet Machines 7	PS1-4-9	9	C000482	Electromagnetic Performance Comparison of Dual-Rotor Permanent Magnet Motor with Three Different Rotor Topologies
36	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-1	1	C000708	Research of the variable frequency compressor motor based on air grooves of rotor yoke
37	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-2	2	C000107	Design of an Adjustable-Performance Internal Permanent Magnet Motor for DC Inverter Compressors used in Airconditioning Systems
38	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-3	3	C000269	Research on Design and Electromagnetic Characteristics Analysis of Super Premium Efficiency (IE4) Permanent Magnet Assisted Synchronous Reluctance Motor for Rare Earth Permanent Magnet Reduction
39	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-4	4	C000481	High Slot Fill Aluminum Distributed Winding for High-Speed and High Power Density Electric Machines
40	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-5	5	C000680	Feasibility Analysis and Sizing for High-Speed IPMSM Designs
41	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-6	6	C000068	Rotor Stress Analysis for High-Speed PM Machines Considering Fringe Effect
42	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-7	7	C000832	Design and Analysis of Fault-Tolerant IPM Considering Bidirectional Electromagnetic- Thermal Coupling Constraints
43	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-8	8	C000290	Investigation of Multi-phase Electric Motors Having the Same Electromagnetic Structure Considering Performance Trade-off
44	Poster	November 27	FIT Arena	13:00-14:00	PS1-5	Permanent Magnet Machines 8	PS1-5-9	9	C000106	Pulsation Reducing Effect in DC Current and Torque for Motor Fault-tolerance Based on Second Order Component Power Cancelation
45	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-1	1	C000018	Improved MTPA Control Strategy with Adaptive Gain for Permanent Magnet Synchronous Reluctance Motors
46	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-2	2	C000534	Modified Virtual Signal Injection Control of MTPA for IPMSM Considering Switching Operating Conditions
47	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-3	3	C000159	Accurate MTPA Control Based on Ferrari Method for IPMSM with Partial Derivative Term Calculation
48	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-4	4	C000558	A Loss Minimization Dynamic-Static Transition Control Strategy Based on Model Predictive Current Control for IPMSMs
49	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-5	5	C000474	Position Offset Injection based Fast and Accurate Maximum Torque Per Ampere (MTPA) Control of Interior PMSMs
50	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-6	6	C000207	Auto Associative Kernel Regression Data- Driven Method for Permanent Magnet Synchronous Motor Control
51	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-7	7	C000570	Comparative Analysis of PID, Self-Tunning PID, and Adaptive Neuro-Fuzzy Logic Inference System Controllers for BLDC Motor Speed Control
52	Poster	November 27	FIT Arena	13:00-14:00	PS1-6	PM Machine Control and Drives 1	PS1-6-8	8	C000707	IPOA-NLADRC Based Permanent Magnet Synchronous Motor Control Strategy
53	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-1	1	C000162	Control Strategy for Small DC-link Capacitor Brushless DC Motor Drives Using a Single DC-link Current Sensor
54	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-2	2	C000360	An Open-winding Permanent Magnet Synchronous Motor Drive System Based on The CSI-VSI Hybrid Converter
55	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-3	3	C000021	Research on Fractional-order Active Disturbance Rejection Control Method for Permanent Magnet Synchronous Motor
56	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-4	4	C000115	Multi-Vector Model Predictive Control for Permanent Magnet Synchronous Motors With Disturbance Compensation
57	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-5	5	C000020	An Improved Active Disturbance Rejection Control for Speed Control of Permanent Magnet Synchronous Motor Using Reduced-order Extended State Observer
58	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-6	6	C000547	Improved Sliding Mode Control Strategy with Disturbance Compensation for PMSM Speed Regulation System

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59	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-7	7	C000187	Current Sampling Error Suppression Method for Deadbeat Predictive Direct Speed Control Based on Quasi- Resonant Controller
60	Poster	November 27	FIT Arena	13:00-14:00	PS1-7	PM Machine Control and Drives 2	PS1-7-8	8	C000308	High-efficiency Drive Technology for High-speed, Multi-pole Motors with Minor Sampling Process
61	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-1	1	C000846	Rotor Position Error Compensation for Sensorless Control of SPMSM Based on BP Neural Network
62	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-2	2	C000885	A Sensorless Control Method for an Open- Phase Five-Phase PMSM by Using Series-SOGI and an Adaptive Neutral-Voltage Compensation
63	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-3	3	C000047	Sensorless Control of SPMSM With Improved Extended Kalman Filter Based on Runge-Kutta Model
64	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-4	4	C000519	Second Order Generalized Integrator Filtering For Enhanced Sliding Mode Observer With Fuzzy Logic Switching Function
65	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-5	5	C000592	Sensorless Active Disturbance Rejection Control of PMSM Based on Extended Kalman Filter
66	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-6	6	C000153	Full-order Super-twisting Non-singular Terminal Sliding Mode Observer for PMSM Sensorless Control
67	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-7	7	C000549	A Nonlinear Flux Observer Based on Limit Cycle Oscillator for Sensorless Permanent Magnet Synchronous Motor Drives
68	Poster	November 27	FIT Arena	13:00-14:00	PS1-8	Sensorless Control (I)	PS1-8-8	8	C000794	Multiple Signal Classification Method of EMF- Based Speed and Position Estimation for Surface PMSM Sensorless Drives
69	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-1	1	C000627	Extended Describing Function Method based Modeling Technique for Three-port Series Resonant Converters
70	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-2	2	C000753	Power Decoupled VSG Based on Full-state Feedback for Better Dynamic Performance and Improved System Robustness
71	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-3	3	C000754	Study on Phase-Change Cooling for A Reactor Used in Offshore Wind Power Converters
72	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-4	4	C000650	Optimal Placement and Sizing of Hybrid Distribution Transformers in Active Distribution Networks Under Load and PV Generation Uncertainty
73	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-5	5	C000198	MPPT control method for micro wind turbine system with Newton method
74	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-6	6	C000330	Performance Improvement of a Magnus Effect- Based Turbine Generator for a Point Absorber Wave Energy Converter
75	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-7	7	C000774	Design of Direct Drive Dual 3-phase Permanent Magnet Generator for Ship-Mounted Wind Power Applications considering Redundancy
76	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-8	8	1 (:000/93	Power Fluctuation Suppression Under Distorted Grid Voltage in Wind Power System Using Wound Rotor Induction Generator
77	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-9	9	C000362	Comparative Study of Operating Characteristics of Doubly-fed Variable-Speed Pumped Storage Unit under Two Different Control Strategies
78	Poster	November 27	FIT Arena	13:00-14:00	PS1-9	Power Converters of Renewable Energy Systems 1	PS1-9-10	10	C000859	Combined capacity and internal resistance estimation of lithium-ion batteries based on voltage recovery
79	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-1	1	C000358	Loss Evaluation of Three-Phase Inverter Driven Two-Phase PWM Scheme at High Switching Frequency
80	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-2	2	C000678	An Overview of Resonant DC-Link Inverters
81	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-3	3	C000109	Robotic Grasp Detection Method Based on A Novel Multi-scale Multi-task Mutual-Learning Architecture in Neural Network A Study on Giant Magnetostrictive Actuator for interior Sound Control System of the Ottra- compact Mobility.
82	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-4	4	C000157	Fundamental Consideration on Formation of the Giant Magnetostrictive Phases Depending on Heat Treatment
83	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-5	5	C000861	Topology Optimization for a Spoke-Type Permanent Magnet Synchronous Motor Based on a Siamese Convolutional Network
84	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-6	6	C000883	Contact Tip Trajectory in Steady-State Regime Prediction Using Deep Learning for Piezoelectric Actuators
85	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-7	7	C000082	Efficiency Map Versus Time-Stepping Solutions for Drive Cycle Performance Analysis of Permanent Magnet Synchronous Motors
86	Poster	November 27	FIT Arena	13:00-14:00	PS1-10	Power Converters of Motor Drives	PS1-10-8	8	C000214	Maximum Torque per Ampere Control of IPMSM Drive for Electric Two-Wheeler Applications
87	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-1	1	C000718	Robust Design Considering Assembly Imperfection of 20 W Chip Mounter Motor

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88	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-2	2	C000098	Design and Analysis of Service Robot Motor with High Torque and High Back drivability Focusing on the Torque/Inertia Ratio
89	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-3	3	C000800	Impact of Partially Demagnetized Permanent Magnets on Operating Range of an Interior Permanent Magnet Synchronous Machine
90	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-4	4	C000252	Selection and Analysis of Rotor Structure for Expansion of IPMSM Operating Range
91	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-5	5	C000319	Analysis and Research on the Influence of Different Rotor Structures on the Magnetic Field Characteristics of Machines
92	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-6	6	C000371	Design And Analysis of Axial Flux Motors with Rotor Mechanical Position Observation Capability
93	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-7	7	C000283	Electromagnetic Reduced Order Model of a Permanent Magnet Synchronous Motor
94	Poster	November 28	FIT Arena	12:00-13:00	PS2-1	Permanent Magnet Machines 9	PS2-1-8	8	C000183	Eddy Current Loss Suppression of Rotor in HSPMSG Considering Skin Effect
95	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-1	1	C000145	Sensorless Rotor Position Estimation and Control for a Three-Stage Synchronous Starter-Generator
96	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-2	2	C000473	Characteristic Analysis of Demagnetizing Fault of Pod Propulsion Motor
97	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-3	3	C000613	Design of Electrically Excited Synchronous Motors for Traction Applications Using Optimisation with Genetic Algorithms
98	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-4	4	C000815	Inductance Measurement of Synchronous Motors with Solid Elements Using Quasi-Static Approach Considering Saturation Effects
99	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-5	5	C000264	Comparison of Hysteresis Motor Output according to Applied Voltage
100	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-6	6	C000265	Torque Ripple Effects according to Hysteresis Motor Closed-Slot Structures Geometry with Finite Element Analysis
101	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-7	7	C000398	Simulation, design and optimization of an electric high-speed motor with distributed tooth- coil winding
102	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-8	8	C000886	A Parallel Hybrid Excitation Brushless Genera- tor Operating Efficiently within Wide-speed Range
103	Poster	November 28	FIT Arena	12:00-13:00	PS2-2	Synchronous Machines 2	PS2-2-9	9	C000559	Research on a New Topology of Asynchronous Excitation Three Stage Brushless Generator without Rotating Rectifier
104	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-1	1	C000467	Temperature-Rise Determination Test for Synchronous Reluctance Machines Applying Superposition and Equivalent-Loading Methods
105	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-2	2	C000103	Design and Optimization of a Ferrite Assisted Synchronous Reluctance Motor for New Energy Vehicles
106	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-3	3	C000118	Design and Verification of IE6 Ultra Efficiency Line-start Permanent Magnet Assisted Synchronous Reluctance Motor
107	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-4	4	C000461	Axial Design Guidelines for Torque Ripple Reduction in Additively Manufactured Synchronous Reluctance Rotors
108	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-5	5	C000827	Assessments of Permanent-Magnet-Assisted Synchronous Reluctance Motors for Electric Forklift Applications in Severe Operational Environments
109	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-6	6	C000479	Static torque characteristics of SRM with a Three-Dimensional Gap Structure
110	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-7	7	C000740	Fault-Tolerant Control for Power Converter in Switched Reluctance Motor (SRM) Applications
111	Poster	November 28	FIT Arena	12:00-13:00	PS2-3	Reluctance Machines 2	PS2-3-8	8	C000624	Performance Evaluation of Novel Segmental Rotor Switch Reluctance Motor with Magnetic Bridge
112	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-1	1	C000100	Method for enhancing the stability margin of the magnetic bearing-rotor system based on a novel low frequency phase shifter
113	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-2	2	C000113	Study of the basic charging characteristics in the vertical linear vibration power generator
114	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-3	3	C000163	Study of Pitching Suppression in a Propulsion and Levitation Integrated Conveyance System Using the Linear Stepper Motor
115	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-4	4	C000244	Non-contact Hanging for Flexible Steel Plate by Magnetic Levitation: Investigation on Levitating Characteristics in Stationary State
116	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-5	5	C000266	Placement of Electromagnets for Edge- supported Maglev Systems: Experimental Study on the Relationship between Steady Current and Vibration Characteristics during Electromagnet Direction Change

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117	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-6	6	C000267	Improvement Technology of Driving- environment Using Two-degree-of-freedom Active Seat Suspension: Design of Ride Comfort by Vibration Control Using Voice Coil Motor
118	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-7	7	C000268	Non-contact Magnetic Suspension for Edge of Flexible Steel Plate: Experimental Consideration on Stable Levitation
119	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-8	8	C000278	Vibration Control for Flexible Steel Plate during Magnetic Suspension: Suppression of Two-degree-of-freedom Vibration by Edge Supported System
120	Poster	November 28	FIT Arena	12:00-13:00	PS2-4	Linear Drives and Magnetic Levitations 3	PS2-4-9	9	C000545	Influence of Blade row Stages on the Pumping Speed of Molecular Pump Based on Entire Blade Row Algorithm
121	Poster	November 28	FIT Arena	12:00-13:00	PS2-5	Induction Machine Control and Drives	PS2-5-1	1	C000432	Improvement of Control Mode Switching Method for Copper Loss Reduction of Induction Machines
122	Poster	November 28	FIT Arena	12:00-13:00	PS2-5	Induction Machine Control and Drives	PS2-5-2	2	C000293	Initial Speed Estimation Method for Induction Motors using Regression Analysis and Self-Excited Vibration Phenomenon
123	Poster	November 28	FIT Arena	12:00-13:00	PS2-5	Induction Machine Control and Drives	PS2-5-3	3	C000878	A Novel Speed Measurement Algorithm Based on Linear Extended State Observer for Segmented Linear Induction Motors with Cooperative Control
124	Poster	November 28	FIT Arena	12:00-13:00	PS2-5	Induction Machine Control and Drives	PS2-5-4	4	C000643	An Improved PLL Control Method for DFIG Under Asymmetric Faults
125	Poster	November 28	FIT Arena	12:00-13:00	PS2-5	Induction Machine Control and Drives	PS2-5-5	5	C000890	Transient Control of Grid-forming Doubly-fed Induction Generator Considering Power Angle Stability and Fault Current Limitation
126	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-1	1	C000433	An Open-Circuit Fault Diagnosis Method for Single Switch of Controlled Rectifier in Doubly Salient Electromagnetic Generator System
127	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-2	2	C000165	Reduction of Iron Loss and Back EMFs of the Doubly Salient Synchronous Reluctance Motor by Estimation of Flux Linkage
128	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-3	3	C000654	The Loss-Minimizing Control Strategy for DSEM Driving System with Current Source Converter
129	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-4	4	C000366	A High Frequency Square Wave Harmonic Excitation Control Strategy for Self-Excited Synchronous Motors
130	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-5	5	C000778	A Novel Brushless Excitation System Capable of Bipolar Field Current Control from the Stator of Electrically/Hybrid-Excited Synchronous Motor
131	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-6	6	C000137	Robust Current Predictive Control of Synchronous Reluctance Machines Considering Magnetic Saturation
132	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-7	7	C000209	Efficiency Optimization Control Strategy for Synchronous Reluctance Motor Considering Iron Loss
133	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-8	8	C000763	Adaptive Dead-Time Algorithm to Reduce Current Harmonics in Three-Phase Motor Inverters Used for Electric Vehicles
134	Poster	November 28	FIT Arena	12:00-13:00	PS2-6	Synchronous Machine Control and Drives	PS2-6-9	9	C000261	Study on Minimization of Smoothing Capacitor by Increasing Response of Power Supply Converter
135	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-1	1	C000231	Robust Model Predictive Control Based on Linear Fitting for Surface-Mounted Permanent Magnet Synchronous Motor
136	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-2	2	C000892	A Feedback-Error-Driven Method for Deadbeat Model Predictive Control Algorithm of PMSM
137	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-3	3	C000477	Quantitative Neutral Point Voltage Balance- based Modulated Model Predictive Control for Three-Level NPC Inverter-fed PMSM Drive
138	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-4	4	C000657	A Modified Modulation Strategy for a Five- Level Inverter Based Open-End Winding PMSM With Floating Capacitor
139	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-5	5	C000169	Model-free current predictive control of permanent magnet synchronous motor based on ultralocal model
140	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-6	6	C000414	Optimized Predictive Power Control of PMSG with Horizon Disturbance Observer
141	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-7	7	C000891	Multi-motor coordinated control system of outer rotor permanent magnet synchronous motor
142	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-8	8	C000314	Implementation of Two-Wheel Independence Drive System Based on Indirect Field-Oriented and Direct Torque Control Strategies
143	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-9	9	C000527	PMSM Characteristics comparison of Rheostatic brake Circuit differences targeted for Electric Hybrid Aircraft
144	Poster	November 28	FIT Arena	12:00-13:00	PS2-7	PM Machine Control and Drives 3	PS2-7-10	10	C000607	Compensation of Speed Synchronization Error of 4-wheel Distributed Drive System Based on Fuzzy PI and Virtual Axis-deviation Coupling Control
145	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-1	1	C000535	A Robust Control Strategy for Enhanced Performance of Multiphase PMSM

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146	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-2	2	C000784	An Improved Deadbeat Direct Torque and Flux Control of Five-Phase Permanent Magnet Synchronous Motor
147	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-3	3	C000868	Direct Torque Control System of Dual Three- Phase PMSM with Load Torque Observer
148	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-4	4	C000737	Order Reduction-Based Fault-Tolerant Decoupling Control for Dual Three-Phase PMSM with Two-Phase Open-Circuit Fault
149	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-5	5	C000674	Fault-Tolerant Control Strategies for Dual Three-Phase Permanent Magnet Synchronous Machine with YASA Topology under Open- Circuit Faults
150	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-6	6	C000884	Research on Fault-tolerant Control Strategy of Dual-Winding Permanent Magnet Synchronous Motor
151	Poster	November 28	FIT Arena	12:00-13:00	PS2-8	Multi-winding/Multi-phase Machine Control	PS2-8-7	7	C000828	Fault-tolerant Control Strategy for Single- phase Open Circuit Fault for Six-phase Doubly Salient Electromagnetic Machine
152	Poster	November 28	FIT Arena	12:00-13:00	PS2-9	Power Converter 1 (DC-DC)	PS2-9-1	1	C000056	Fuzzy Neural Nonsingular Terminal Sliding Mode Control of DC-DC Buck Converter
153	Poster	November 28	FIT Arena	12:00-13:00	PS2-9	Power Converter 1 (DC-DC)	PS2-9-2	2	C000062	Complete Soft Switching Implementation Based on LCC-LCC Compensation Network for Wireless Power Transfer System
154	Poster	November 28	FIT Arena	12:00-13:00	PS2-9	Power Converter 1 (DC-DC)	PS2-9-3	3	C000743	Power Optimization Strategy for Buck circuits based on Digital Twins
155	Poster	November 28	FIT Arena	12:00-13:00	PS2-9	Power Converter 1 (DC-DC)	PS2-9-4	4	C000354	Back-flow Power Optimization Strategy of DAB Converter with Extended Phase Shift Control
156	Poster	November 28	FIT Arena	12:00-13:00	PS2-9	Power Converter 1 (DC-DC)	PS2-9-5	5	C000168	DC-Link Capacitor Lifetime Extension for Two-Level Back-to-Back Converters Based on Zero-Sequence Voltage Injection
157	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-1	1	C000088	A New Hybrid Modulation Method with Low Current Distortion and Switching Losses for Single-Phase Three-Level Inverters
158	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-2	2	C000446	Improved Capacitor Voltage Balancing Method for CHB Inverter Based on Hybrid Modulation Strategy and Reference Voltage Reconfiguration
159	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-3	3	C000229	Carrier-based Discontinuous PWM Strategy by Switching Clamp Modes for Vienna Rectifier With Unbalanced DC- Links
160	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-4	4	C000512	Control of Quick Charger System applying MMC with High Frequency AC output
161	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-5	5	C000791	A Compact Hybrid Multilevel Converter With Wide Operation Range
162	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-6	6	C000833	Control of variable speed pumped storage unit based on power electronic transformer under unbalance of power grid voltage
163	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-7	7	C000324	Preparation of a Technical Paper for ICEMS 2024 Proceedings
164	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-8	8	C000434	Common Mode Voltage Suppression Method for Third-Harmonic Injection Two-Stage Matrix Converter in Low Modulation Ratio
165	Poster	November 28	FIT Arena	12:00-13:00	PS2-10	Power Converter 2 (AC-DC, DC-AC)	PS2-10-9	9	C000500	IPF Improvement of DPWM-controlled for DMC with A Double PI Controller
166	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-1	1	C000546	Design and Optimization of a Permanent Magnet biased Hybrid Magnetic Bearing for Turbo-molecular Pump
167	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-2	2	C000582	Model Calibration of Inconsistent Coils Shape Driven by Coupling Effect of Magnetic Levitation Planar Motor
168	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-3	3	C000614	Influence of Secondary Structure on the Transverse Edge Effect of LP-DSLIM
169	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-4	4	C000634	Modal Vibration Control of Magnetic Bearing Rotor System Based on Second Order Generalized Integrator- Gradient Estimator
170	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-5	5	C000640	Simulation of Vibration Characteristics of Magnetically Levitated Steel Plate under Disturbance Condition
171	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-6	6	C000679	Analysis and control of self-sensing model of isolated axial magnetic bearing
172	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-7	7	C000880	Structural Optimization Design of Permanent Magnet Linear Force Motor for Aviation
173	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-8	8	C000104	The Method of Single-Segment Layer-by-Layer Substitution for Inverse Design of Passive Magnetic Springs
174	Poster	November 28	FIT Arena	13:00-14:00	PS3-1	Linear Drives and Magnetic Levitations 4	PS3-1-9	9	C000842	Research on Optimization Design of Double- sided Consequent-pole Permanent Magnet Synchronous Linear Motor

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175	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-1	1	C000750	Investigation of Design Methods to Improve the Performance of a Motor Which Is Capable of Switching between WFFSM Drive and SynRM Drive
176	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-2	2	C000605	Study on Pole-Slot Combinations of Half-Wave Rectified Variable Field Flux Motor with Axial Gap Structure
177	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-3	3	C000612	Experimental Validation of a Six-Pole Half- Wave Rectified Variable Field Flux Motor
178	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-4	4	C000699	Design Study on Hybrid Excitation Generator for Micro-hydroelectric System
179	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-5	5	C000739	Comparison of Variable Flux Memory Machine and Double-Variable Flux Memory Machine with Hybrid Magnetic Circuits
180	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-6	6	C000745	Design and Analysis of Variable Flux Motor with Rotatable Magnet
181	Poster	November 28	FIT Arena	13:00-14:00	PS3-2	Flux Switching & Variable Flux Machines 2	PS3-2-7	7	C000027	Field Unit Type Magnet-Assisted Wound Field Motor for HEV and EV Applications with Distributed Mortise Structure
182	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-1	1	C000299	Precise Prediction of Air-gap Magnetic Harmonics for IPMSM Based on Improved Magnetic Field Modulation Theory
183	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-2	2	C000302	A novel equivalent magnetic network method for permanent magnet vernier motor
184	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-3	3	C000599	Scaling Effect Analysis of Surface-Mounted Permanent Magnet Vernier Machine with Concentrated Windings
185	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-4	4	C000836	A Novel Consequent-Pole Vernier Permanent Magnet Machine With Dual Armature Winding Configuration
186	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-5	5	C000819	A High Strength and Low Cogging Torque Modulator Structure for Magnetic-geared Machines
187	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-6	6	C000575	Optimization of Repulsion Cycloidal Magnetic Gear with Inset Radial Magnets
188	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-7	7	C000130	A Novel Model for Hybrid Stepper Motors Considering Magnetic Saturation
189	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-8	8	C000063	Comparative Analysis of Tangentially Magnetized Stator-Permanent-Magnet Hybrid Stepping Machines with Four, Five and Six-Tooth
190	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-9	9	C000080	Experimental verification of distribution factors in counter-rotating twin harmonic PM machines
191	Poster	November 28	FIT Arena	13:00-14:00	PS3-3	Special Machines	PS3-3-10	10	C000133	A Novel High-Speed Solid Rotor Induction Motor with Equidirectional Toroidal Rectangular Winding
192	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-1	1	C000053	Analysis of Fundamental Electromagnetic Performance of Stator Permanent Magnet Bearingless Slice Motor Topology
193	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-2	2	C000110	Proposal of pediatric centrifugal pump type ventricular assist device using a bearingless motor
194	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-3	3	C000322	Reduction of Force Error Angle by Flux- Strengthening Control in Two-axis Actively Positioned Bearingless PM Motor
195	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-4	4	C000346	Characteristics Analysis of Novel Permanent Magnet Biased Bearingless Switched Reluctance Motor
196	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-5	5	C000388	Variable Gain Control of Nonlinear Suspension Force for Bearingless Doubly Salient Electromagnetic Motor Under Magnetic Saturation
197	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-6	6	C000438	Sensorless control of PMa-BSynRM based on ISWATS adaptive neural network left inverse soft-sensing technique
198	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-7	7	C000475	Calculation of Eddy Current Loss in Surface Permanent Magnet Rotor Due to Suspension Flux in High Power Bearingless Motors
199	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-8	8	C000513	Decoupling of Magnetic Circuits between Combined Radial-Axial Magnetic Bearing and Permanent Magnet Bearingless Motor
200	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-9	9	C000542	Comparison and Design Optimization of Consequent-Pole and Multi-Monopole Surface Permanent Magnet Bearingless Motors
201	Poster	November 28	FIT Arena	13:00-14:00	PS3-4	Bearingless Machine 2	PS3-4-10	10	C000847	Optimization Design of Hybrid Excitation Bearingless Permanent Magnet Synchronous Generator
202	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-1	1	C000404	Maximum Torque Per Ampere Control of Variable Flux Memory Motor Based on Online Parameter Identification
203	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-2	2	C000489	Position Offset Injection based Winding and Permanent Magnet Temperature Decoupled Estimation for PMSMs

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204	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-3	3	C000852	Multi-objective Optimization Three-Vector-Based Model Predictive Current Control with Adaline Online Parameter Identification for PMSM Drives
205	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-4	4	C000260	Fundamental Study of On-Line Inductance Identification for IPMSM
206	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-5	5	C000869	The Full Rank Identification of DTP-PMSM Parameters
207	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-6	6	C000641	Online Parameters Identification for an IPMSM Based on Extended Kalman Filter
208	Poster	November 28	FIT Arena	13:00-14:00	PS3-5	Parameter Estimation	PS3-5-7	7	C000857	Position Offset and Current Angle Combined Injection based online Multiparameter Estimation of PMSM Considering Inverter Distortion
209	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-1	1	C000060	A Novel SMO Based Diagnosis Method for Interturn Short-Circuits in SRM by Unaligned Inductance Identification
210	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-2	2	C000085	Levitation Displacement Control of Bearingless Switched Reluctance Motor With UDE-based Method
211	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-3	3	C000328	Research on Direct Instantaneous Torque and Suspension Force Control Strategy for Stepped Rotor Bearingless Switched Reluctance Motor
212	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-4	4	C000617	Validation of Variable Voltage Control Method Using Z-Source Inverter for SRM Drive
213	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-5	5	C000841	High-Performance Starting Control Strategy for Switched Reluctance Starter/Generator
214	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-6	6	C000894	LADRC-based high dynamic Control Strategy for SRM-based EMA System
215	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-7	7	C000202	Research on voltage stabilizing system of switched reluctance motor based on fuzzy PID control
216	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-8	8	C000029	Fault-Tolerant Sensorless Control Method Based on Multiple Second Order Generalized Integrator for SRM Drives
217	Poster	November 28	FIT Arena	13:00-14:00	PS3-6	Switched Reluctance Machine Control and Drives	PS3-6-9	9	C000164	An Inductance-Slope-Based Sensorless Control Method for Switched Reluctance Motor
218	Poster	November 28	FIT Arena	13:00-14:00	PS3-7	Torque Ripple Suppression Control	PS3-7-1	1	C000895	Torque Ripple Suppression Strategy Based on Quasi-resonant Active Disturbance Rejection Control for PM/RHR-DSLSSM
219	Poster	November 28	FIT Arena	13:00-14:00	PS3-7	Torque Ripple Suppression Control	PS3-7-2	2	C000906	Torque Ripple Reduction Control of Axial Rotor-staggered Permanent Magnet Reluctance Motor Using Nonlinear Extend State Observer
220	Poster	November 28	FIT Arena	13:00-14:00	PS3-7	Torque Ripple Suppression Control	PS3-7-3	3	C000772	A Novel Torque Ripple Mitigation Control Method for Single-Phase PMSM Based on Virtual Multi-Phase Algorithm
221	Poster	November 28	FIT Arena	13:00-14:00	PS3-7	Torque Ripple Suppression Control	PS3-7-4	4	C000123	Harmonic Injection-based Torque Ripple Suppression Strategy for Synchronous Reluctance Motor
222	Poster	November 28	FIT Arena	13:00-14:00	PS3-7	Torque Ripple Suppression Control	PS3-7-5	5	C000602	Torque Ripple Suppression Control Using Parallel Resonant Controller and ANN in Position and Acceleration Sensorless Control of Stepping Motor
223	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-1	1	C000245	Bidirectional SP-type Wireless Power Transfer System Based on Parity-Time Symmetry Condition
224	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-2	2	C000271	Determination Scheme of Ferromagnetic Metal Objects Using Detection Coil in Wireless Power Transfer
225	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-3	3	C000333	Estimation of Transmitter Inductance on Foreign Object in Wireless Power Transfer
226	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-4	4	C000405	Frequency-based Power Distribution via Virtual AC Bus For Dual-frequency Wireless Energy Router System
227	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-5	5	C000755	Power Factor Improvement Control of Variable Active Capacitor System for Wireless Power Transfer
228	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-6	6	C000777	A Vehicle-to-Vehicle (V2V) Mode in Multi- Receiver WPT System Utilizing Transmitting Loop from Primary Compensation Circuit
229	Poster	November 28	FIT Arena	13:00-14:00	PS3-8	Power Converter 3 (WPT)	PS3-8-7	7	C000792	Wireless Power Transfer System for Multiple Drones In-Flight Charging Applications Under Wide Charging Tolerance with Constant Charging Current
230	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-1	1	C000212	Time-Efficient Power Loss Calculation for Battery-Electric Powertrains Based on Harmonic Loss Models
231	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-2	2	C000493	Active Power Decupling Strategy for Integrated Single-Phase Charging System of EVs with Dual-Battery
232	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-3	3	C000407	Modeling and Control of a Hybrid Power System for Electric Propulsion Aircraft

No	Туре	Date	Room	Time	Session ID	Session Title	Presentation ID	Order	Submission no	Paper Title
233	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-4	4	C000554	A Capacity Planning Method for EV Charging Stations Based on Fuzzy C-means Clustering and Deep Extreme Learning Machine
234	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-5	5	C000571	CFD Thermal Analysis of Axial-Flux Permanent Magnet Synchronous Motor with Water Cooling Channels for Underwater Propulsion Applications
235	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-6	6	C000747	Design of a 100 kW SPMSM for Podded Propulsion and Multiphysics Analysis of Fault Operating Simulation
236	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-7	7	C000712	Analysis of the Battery Capacity and Imbalanced Charging Ability for a Cascade H Bridge in Shinkansen Regeneration Energy Storage Application
237	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-8	8	C000028	Mass Reduction of a PMSM Through Segmented Stator and Material Mix by Holistic Drivetrain Consideration
238	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-9	9	C000025	Sliding Mode Control Method Based on FLC for Performance Improvement of PMD Battery Charger
239	Poster	November 28	FIT Arena	13:00-14:00	PS3-9	Power Electronics of Mobility Applications	PS3-9-10	10	C000227	Solution of Active Safety for Virtual Track Train Based on RRT* and MPC
240	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-1	1	C000529	Improved Current Limiting Control for LVRT Strategy of Virtual Synchronous Generator
241	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-2	2	C000530	Generic Algorithm Based Parameter Optimization for an S-SP Compensation Topology Based Inductive Power Transfer System
242	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-3	3	C000532	A Variable-Frequency and Phase-Shifted Based Current Sharing Control for Parallel LLC Reso- nant Converters with Parameter Differences
243	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-4	4	C000594	A Half Controlled Current Source Actively Commuted Converter With the Low Switching Frequency Modulation Strategy
244	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-5	5	C000687	Suppression of second harmonic current by active power decoupling circuit based on bus voltage feedforward
245	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-6	6	C000719	Investigation on Error Decomposition-based Feedback Control Strategy
246	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-7	7	C000829	Multi-Objective Coordinated Control of Permanent Magnet Direct-Drive Wind Power System Under Asymmetrical Grid Fault
247	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-8	8	C000877	Current Harmonic Suppression Strategy for Grid-Connected NPC Converters at Low Switching Frequencies
248	Poster	November 28	FIT Arena	13:00-14:00	PS3-10	Control of Power Converter	PS3-10-9	9	C000155	Fault-Tolerant Strategy for More Reliable Cascaded H-Bridge Inverters
249	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-1	1	C000250	Fast Steady-State Analysis Method for Cage Induction Motors Based on Polyphase TP-EEC Method in a Rotational Reference Frame
250	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-2	2	C000586	Analysis of electromagnetic force and power consumption in magnetic levitation planar motor with dual-layer coil array
251	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-3	3	C000848	Dynamic Behavior of levitated Flexible Steel Plate in Bending Electromagnetic Levitation System during Disturbance Input
252	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-4	4	C000858	Magnetic Properties of Iron Core Materials Based on the Creep Model and Dynamic Observation of Magnetic Domains
253	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-5	5	C000896	Improvement of a Magnetostrictive Model Considering Applied Stress and Magnetic Fields Including Hysteresis Effects
254	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-6	6	C000520	A Novel Electromagnetic Analysis Method of Spoke-type Permanent Magnet Machine with Overhang Structure
255	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-7	7	C000621	Simulation Analysis of Air Cooling System Flow Field Characteristics for Generator-Motor in Pumped Storage Power Stations
256	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-8	8	C000419	Electromagnetic-Structural Coupled Analysis of Magnetic-Elastic Power Generation System with High Load and Small Deformation Characteristics
257	Poster	November 29	FIT Arena	12:00-13:00	PS4-1	Numerical Analysis and Modeling 2	PS4-1-9	9	C000897	Frequency Response Analysis for Transformer Winding with Improved Equivalent Circuit
258	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-1	1	C000427	Probabilistic Analysis of Partial Discharges in the Stator Winding Insulation for Electrified Aviation
259	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-2	2	C000649	Fast and accurate radial-flux PMSM step- skewing computation methodology for NVH improvements across the machine full operation range
260	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-3	3	C000077	Investigation of Measurement Method for Thickness of Hot Springs Scale Using Electromagnetic Force Vibration
261	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-4	4	C000084	A Negative Stiffness Injection Method for PMSM in the Five-DoF Magnetic Levitation System to Suppress the Vibration

No	Туре	Date	Room	Time	Session ID	Session Title	Presentation ID	Order	Submission no	Paper Title
262	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-5	5	C000182	Novel Online Non-invasive Measurement Approach for PMSM-Transmission Chain Radial Natural Frequency Based on Driving PMSM Radial Force Injection
263	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-6	6	C000408	A Novel Partial Slot Unwounded Method for Electromagnetic Vibration Reduction of Large Electric Machines
264	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-7	7	C000450	A Motor Vibration Suppression Method Based on Vibration Reduction Coils
265	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-8	8	C000701	Multi-mode Vibration Suppression for Electric Machines using Passive Dynamic Vibration Absorbers Mounting on Stator Outer Peripheral
266	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-9	9	C000812	Vibration Reduction by Grooving on Magnets for PMSMs
267	Poster	November 29	FIT Arena	12:00-13:00	PS4-2	Noise, Vibration and Reliability of Electric Machines 2	PS4-2-10	10	C000033	Combined Fault Diagnosis of Stator and Rotor Windings in a PWM Inverter-Fed Induction Motor Using Frequency Spectrum of Estimated Air-Gap Torque
268	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-1	1	C000030	Study on the Design Optimization of Cast- Resin Transformer using Permutation with Repetition and Python's Scipy Method
269	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-2	2	C000087	Optimal Design of Three-Phase Transformer using Genetic Algorithm and FEMM
270	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-3	3	C000449	Additive Manufacturing Lightweight Inductor
271	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-4	4	C000557	Influence of Distorted Voltage and Harmonics on High-frequency Transient Model of Transformers
272	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-5	5	C000786	Core Loss Calculation of Nanocrystalline High- Frequency Transformer under Non-Sinusoidal Excitation
273	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-6	6	C000830	Analysis of Inter-turn Short-circuit Characteristics in Single-phase Traction Transformers Based on Digital Twin
274	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-7	7	C000173	The Basic Study on the Optimization of Mutual Induction Circuit that Separates Zero Energy into Positive and Negative Energy
275	Poster	November 29	FIT Arena	12:00-13:00	PS4-3	Transformers and Power Apparatus	PS4-3-8	8	C000352	A Proposal of a New Temperature Rise Test Method for Filter Reactors — Middle-Frequency Test —
276	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-1	1	C000422	Investigation on the Torque to Mass Ratio of Synchronous Magnetic Couplings
277	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-2	2	C000237	A hybrid spiral stepper motor with staggered punching structure
278	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-3	3	C000397	Design and Optimization of Non-Insulated Pipe Wall Electromagnetic Flowmeter for High-Temperature Liquid Metal Flow Measurement
279	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-4	4	C000538	Parameter Optimization Design of Magnetic Levitation Centrifugal Blood Pump Based on Parameter Sensitivity Analysis
280	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-5	5	C000606	Energy-Saving Power Transmission Device for CNC
281	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-6	6	C000090	Detection of Slot Discharges by using On-line PD Monitoring System with a Non-contact Sensor
282	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-7	7	C000522	Analysis and Control Strategy Study of Large- scale Pumped Storage Power Station Phase Modulation Operation
283	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-8	8	C000347	Model Predictive Control with Disturbance Compensation for Trajectory Tracking of Three- degree-of-freedom Spherical Joint Actuator
284	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-9	9	C000837	Efficiency Improvement of Induction Motors with Novel Magnetic Slot Wedges
285	Poster	November 29	FIT Arena	12:00-13:00	PS4-4	Other Related Topics in Electric Machines	PS4-4-10	10	C000376	Improvement of Shape Memory Alloy (NiTi) Actuation Frequency Using Highly Thermally Conductive Metal Layer
286	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-1	1	C000389	Improved Synchronous Demodulation Method for Three-stage Synchronous Machine Based on D-axis Response High-Frequency Voltage
287	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-2	2	C000821	Improved Sensorless Control of IPMSM Drives Using Complex Bandpass Filter and Pseudolinear Enhanced PLL
288	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-3	3	C000174	Model Predictive Sensorless Control with High-Frequency Square-Wave-Type Voltage Synchronized with Carrier
289	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-4	4	C000285	Position Sensorless Control in Low-Speed Regions for Non-Saliency and Concentrated Winding Motors
290	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-5	5	C000552	Position Sensorless Control of Dual Three-Phase PMSM Based on Improved Sliding Mode Observer

No	Туре	Date	Room	Time	Session ID	Session Title	Presentation ID	Order	Submission no	Paper Title
291	Poster	November 29	FIT Arena	12:00-13:00	PS4-5	Sensorless Control 2	PS4-5-6	6	C000835	A Precise Rotor Flux Estimator for a Sensorless Dual Three-Phase SPMSM
292	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-1	1	C000142	Effects of <ita>d</ita> -axis Inductance Change for Position Sensorless Control of SynRM at Low Velocities by Using an Extended EMF caused by High-frequency Current Superposition
293	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-2	2	C000046	Inductance Linearization Region-Based Initial Rotor Position Estimation Method for Doubly Salient Electromagnetic Motor
294	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-3	3	C000072	Position Estimation for Sinusoidal Doubly Salient Electromagnetic Machine by Injecting High-Frequency Current Signal into Excitation Winding
295	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-4	4	C000437	Research on Initial Rotor Position Estimation for DSEM Based on Excitation Field Building
296	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-5	5	C000560	Position Sensorless Control Method for Doubly Salient Electromagnetic Machine Based on Non-conduct Phase Current Injection
297	Poster	November 29	FIT Arena	12:00-13:00	PS4-6	Sensorless Control 3	PS4-6-6	6	C000312	Reciprocating Drive of Position Sensorless Linear Switched Reluctance Motor Based on Mathematical Model of Magnetization Curves
298	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-1	1	C000531	Design of a Dynamic Compensator for Load-side Speed and Torsional Torque Controls of a Two-inertia System
299	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-2	2	C000769	Simple Design Method of Two-Degree-of- Freedom PID Position Controller Specifying Disturbance Response for Linear Servo Motors
300	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-3	3	C000058	Modeling and Optimal Control for 2-DOF Differential Robot Joint Based on Cascade Extended State Observer
301	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-4	4	C000099	Dual-redundant Electro-mechanical Actuators Force Fight Reduction Control Based on Position Sensor Fault-tolerant
302	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-5	5	C000254	Vibration Suppression Method in Flexible Loads Motor Drives System based on Speed Feedback Resonance Filter
303	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-6	6	C000498	Servo System End-of-System Oscillation Suppression Based on Acceleration Limiting and Notch Filtering
304	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-7	7	C000540	Speed Regulation Strategy of Blood Pump Motor used in Hypothermic Therapy
305	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-8	8	C000548	Servo Motor Control System Design Based on EtherCAT Real-time Communication
306	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-9	9	C000834	Study of Robust Control Strategy for the Levitation Subsystem of Bilateral Long Primary Permanent Magnet Linear Synchronous Motor
307	Poster	November 29	FIT Arena	12:00-13:00	PS4-7	Motion Control and Maglev Control Systems	PS4-7-10	10	C000076	Vibration Suppression Based on Phase Shift Notch Filter for Bearingless Motor Rotor Mass Unbalance System
308	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-1	1	C000149	A Novel Day-ahead Probability Prediction Method for PV Station Based on Improved CNN-Autoformer network
309	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-2	2	C000185	Flexible Resource Data Acquisition and Dynamic Characterization Techniques for Virtual Power Plants with a High Percentage of New Energy Access
310	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-3	3	C000192	Research on Reserve Capacity Planning Method for Distribution Systems Considering Uncertainty of Temperature-Controlled Loads
311	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-4	4	C000436	A Novel Method for Optimal Capacity Configuration of the Grid-Connected Wind- Solar Complementary Power Generation
312	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-5	5	C000619	A Study of Dynamic Characteristics of Series- connected Wind Farm Using a Simulation Model That Can Reduce Computational Load
313	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-6	6	C000723	Multi-time Scale Optimization Scheduling Model for Over-matched PV Station with Energy Storage
314	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-7	7	C000041	A Coupled Analysis of Nonlinear Vibration Energy Harvester Based on Predictor-Corrector Approach
315	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-8	8	C000015	Machine Learning based Methodology for Fast Assessment of Battery Health Status
316	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-9	9	C000213	Fleet Management on Inland Waterways for Electric Boat Ferry System
317	Poster	November 29	FIT Arena	12:00-13:00	PS4-8	Power Converters of Renewable Energy Systems 2	PS4-8-10	10	C000704	A Two-Stage Sorting Method based on Deep Clustering for Retired Lithium-ion Battery Considering Static and Dynamic Consistency
318	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-1	1	C000222	Design of the Hydroelectric Turbine Unit's Evaporative Cooling Automatic Control System
319	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-2	2	C000881	Optimized Configuration Method for Intelligent Terminals Based on Improved Bat Optimization Algorithm

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320	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-3	3	C000882	A Distributionally Robust Optimization Scheduling Method for Cascaded Hydro-PV-Storage Complementary Power System Based on Deep Learning
321	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-4	4	C000031	Advanced Method for Electricity Theft Detection: A Case Study in Low-Voltage Station
322	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-5	5	C000440	A Multi-microgrid Energy Trading Strategy to Achieve Carbon Neutrality
323	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-6	6	C000456	Online Location Approach for Aged Segment of HVDC Cables Using Insertion Index Perturbation and Reflection Analysis
324	Poster	November 29	FIT Arena	12:00-13:00	PS4-9	Power Converters of Renewable Energy Systems 3	PS4-9-7	7	C000197	A Chance-Constrainted Multi-Stage Planning Method for Rural Microgrids Considering Energy Self- sustained ability under Extreme Off-Grid Scenarios
325	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-1	1	C000459	Design and Implementation of Online IGBT Junction Temperature Measurement System for Practical Application in DC/AC Converter
326	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-2	2	C000845	Thyristor-Based Multi-Port DC Solid-State Circuit Breaker Capable of Bidirectional Operation
327	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-3	3	C000329	Development of a New Hybrid Switch with Larger DC Current Breaking Capacity and Longer Lifetime
328	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-4	4	C000395	Emulation of an Inter-Turn Short Circuit with a Variable Fault Resistor
329	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-5	5	C000521	Loss Analysis of Hybrid Switch with Minimum SiC MOSFET Conduction Modulation
330	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-6	6	I C000856	Characterization of Commercial High-Power SiC Modules for Loss Performance in Continuous Operational DAB Applications
331	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-7	7	C000662	Reliability Analysis of Three-Phase Transformer-less UPS using SiC devices
332	Poster	November 29	FIT Arena	12:00-13:00	PS4-10	Power Electronic Devices and Applications	PS4-10-8	8	C000334	Non-Contact Measurement of Defect in the Backside of Steel Plate by Electromagnetic Force Vibration